Given al 
$$2^{24}$$
 order OLF: (LINEAR)  
 $\vec{x} + \vec{c}\vec{x} + \vec{k}\vec{x} = 0$  Fixed point :  $\vec{x} = 0$ .  
Hypothesis (a solution  $\vec{x} = ue^{\lambda t}$   $\vec{x} = vAe^{\lambda t}$   $\vec{x} = vAe^{\lambda t}$ .  
 $\vec{x} + \vec{c}\vec{x} + \vec{k}\vec{x} = 0$   
 $\vec{t}_{10}$   $\vec{t}_{$ 

The statility or otherwise of a fixed point / equilibrium.  
of a nontinear system is "wouldy" (in a serve that with the make.  
precise) determined by analysing the himarization.  
So use first study linear bytems in detail.  
General 2D linear systems:  

$$\frac{dy_1}{dt} = a_1y_1 + a_2y_2 \qquad y = AY = (1)$$

$$\frac{dy_2}{dt} = a_2y_1 + a_2y_2$$

$$\frac{dy_2}{dt} = a_2y_1 + a_2y_2$$

$$\frac{dy_2}{dt} = a_2y_1 + a_2y_2$$

$$\frac{dy_2}{dt} = Ay_2y_1^{t} + a_2y_2$$

$$\frac{dy_2}{dt} = Ay_2y_1^{t}$$

$$\frac{dy_3}{dt} = Ay_2y_1^{t}$$

$$\frac{dy_4}{dt} = Ay_2y_1^{t}$$

$$\frac{dy_2}{dt} = Ay_2y_1^{t}$$

$$\frac{dy_2}{dt} = Ay_2y_1^{t}$$

$$\frac{dy_3}{dt}$$

$$\frac{dy_4}{dt} = Ay_2y_1^{t}$$

$$\frac{dy_4}{dt} = Ay_2y_1^{t}$$

$$\frac{dy_4}{dt}$$

$$\frac{dy_4}{dt} = Ay_2y_1^{t}$$

$$\frac{dy_4}{dt}$$

$$\frac{dy_4}{dt} = Ay_2y_1^{t}$$

$$\frac{dy_4}{dt}$$

$$\frac{dy_4}{$$

$$(a_{11} - \lambda)(a_{22} - \lambda) - a_{12}a_{21} = 0 =) \quad \lambda^2 - \lambda(a_{11} + a_{22}) + (a_{11}a_{22} - a_{12}a_{21}) = 0$$

There are 2 solutions 
$$\lambda_1$$
 and  $\lambda_2$ .  
 $\lambda^2 = A(trace(A)) + der(A) = 0$   
 $\lambda_{1,2} = + trace(A) + \sqrt{[trace(A)]^2 - 4 det(A)}$  with  
2 corresponding  
2 eigenvectors  
Note: We showed that  $\dot{y} = Ay$  is equivalent to  
 $\ddot{z} + (\alpha_{11} + \alpha_{22})\dot{z} + (\alpha_{11}\alpha_{22} - \alpha_{12}\alpha_{21})z = 0$   
 $\ddot{z} - (trace(A))\dot{z} + (det(A))z = 0$   
 $- trace(A) \sim damping / main (con be negative)$   
 $determinant(A) \rightarrow Stiffness / mars (can be negative)$ 

So general solution is  

$$y(t) = a$$
 kinear combination of  $V_1 e^{At}$  and  $V_2 e^{A_2 t}$ .  
 $= k_1 V_1 e^{A_1 t} + k_2 V_2 e^{A_2 t}$   
 $k_1$  and  $k_2$  are constants that can be determined given initial  
Conditions  $Y(0) = \begin{bmatrix} y_1(0) \\ y_2(0) \end{bmatrix}$ .

Let 
$$e = \operatorname{trace}(A)$$
  
 $A = \operatorname{ideterminant}(A)$ .  
 $A_{1,2} = \frac{1}{2}\left(2 \pm \sqrt{2^{k} - 4A}\right)$ .  
Cant1:  $e^{2} - 4A > 0$ .  
 $\Rightarrow A_{1,2}$  REAL.  
Solution Looks Like  $Y(t) = K_{1}Y_{1}e^{A_{1}t} + K_{2}Y_{2}e^{A_{2}t}$ .  
(STABLE).  $Y(t)$  decays to  $\begin{bmatrix} 0 \\ 0 \end{bmatrix}$  in general entry when  
both  $A_{1}$  and  $A_{2}$  are negative.  
 $\begin{cases} 2 + \sqrt{e^{2} - 4A} < 0 \\ 0 \end{bmatrix}$  is general entry when  
both  $A_{1}$  and  $A_{2}$  are negative.  
 $\begin{cases} 2 + \sqrt{e^{2} - 4A} < 0 \\ 0 \end{bmatrix}$  is general entry when  
both  $A_{2}$  and  $A_{3}$  are negative.  
 $\begin{cases} 2 + \sqrt{e^{2} - 4A} < 0 \\ 0 \end{bmatrix}$  is general entry when  
both  $A_{1}$  and  $A_{2}$  are negative.  
 $\begin{cases} 2 + \sqrt{e^{2} - 4A} < 0 \\ 0 \end{bmatrix}$  is general entry when  
both  $A_{1}$  and  $A_{2}$  are negative.  
 $\begin{cases} 2 + \sqrt{e^{2} - 4A} < 0 \\ 0 \end{bmatrix}$  is determined to be interval of the entry of and the entry is and the entry of the

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have



LECTURE 4B / LECTURE 5

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$$\frac{dV}{dk} = AY \qquad A = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix}, \quad Y = \begin{bmatrix} y_1 \\ y_2 \end{bmatrix},$$

$$Y = \lfloor v_{ax}(A) = a_{a} + a_{22},$$

$$X = trace(A) = a_{a} + a_{22},$$

$$A = determinente(A) - a_{11}a_{22} - a_{12}a_{24},$$
STABLE  
is and only if  $T < 0$  and  $A > 0$ .  
UNISTABLE  
if and only if  $T < 0$  and  $A > 0$ .  
UNISTABLE  
if  $T > 0$  or  $A < 0$   
determinent (A) -  $a_{11}a_{22} - a_{12}a_{24},$ 
SUMMARY  
UNISTABLE  
if  $T > 0$  or  $A < 0$   
determinent (A) -  $a_{11}a_{22} - a_{12}a_{24},$ 
SUMMARY  
Not counting  
bounders (Conus.  
Oscillations if  $T^2 - 4A < 0$  (Like underdomped)  
No Oscillations if  $T^2 - 4A < 0$  (Like orderdomped)  
No Oscillations if  $T^2 - 4A < 0$  (Like orderdomped)  
STABLE, GROWIN  
Hitti NO  
OSCILLATIONS  
(UNISTABLE)  
STABLE, DECAY  
WITH OSCILLATIONS.  
 $T^2 - 4A < 0$   
STABLE, DECAY  
No OSCILLATIONS.  
 $T^2 - 4A < 0$   
STABLE, DECAY  
No OSCILLATIONS.  
 $T^2 - 4A > 0$ .  
STABLE, DECAY  
No OSCILLATIONS.  
 $T^2 - 4A > 0$ .

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Example 1

$$\begin{split} \ddot{Y} = AY, \quad A = \begin{bmatrix} A & a \\ o & A_{2} \end{bmatrix} \quad A_{1} \quad and A_{2} \quad trid , \\ \text{Eigenvectors} \quad A_{1} \quad arcd A_{2} \\ \vdots \end{bmatrix} \text{ and } \begin{bmatrix} a \end{bmatrix} \text{ respectively} , \quad V_{1} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad V_{2} = \begin{bmatrix} 0 \\ 1 \end{bmatrix} \\ \text{ Superature serves} \quad \begin{bmatrix} 1 \\ 0 \end{bmatrix} \text{ and } \begin{bmatrix} 0 \\ 1 \end{bmatrix} \text{ respectively} , \quad V_{1} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad V_{2} = \begin{bmatrix} 0 \\ 1 \end{bmatrix} \\ \text{ Superature serves} \quad Y(k) = C_{1} \in A^{1} \quad V_{1} + C_{2} \in A^{2} \quad V_{2} \\ \vdots \\ Y_{1} = A_{1} \otimes A^{2} \end{bmatrix} \implies \begin{cases} y_{1} = y_{1}(0) \in A^{2} \\ y_{2} = y_{1}(0) \in A^{2} \\ y_{3} = y_{3}(0) \in A^{2} \\ y_{3} = y_{3}(0) \in A^{2} \\ y_{3} = y_{3}(0) \in A^{2} \\ y_{3}(k) = y_{3}(0) \\ y_{4}(k) = y_{4}(0) \\ y_{5}(k) = \frac{y_{5}(0)}{y_{5}(k)} \\ y_{5}(k) = \frac$$

The direction of the avious indicate when happens to 
$$\begin{bmatrix} y_1 \\ y_2 \end{bmatrix}$$
  
as time moves forward. Here, wherever you start (whatever  
the initial condition),  $\begin{bmatrix} y_1 \\ y_2 \end{bmatrix} \rightarrow \begin{bmatrix} 0 \\ 0 \end{bmatrix}$  as  $t \Rightarrow \infty$ .

Case 2

CONK 3

22<21<0





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~ Line of fixed points.

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SPECIAL BOUNDARY CASE

E-xomple 2

WHEN THERE ARE NOT ENOUGH EIGENVECTORS

$$\dot{Y} = AY$$
,  $A = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix}$ . Usually, we can find eigenvalues  $A_1$ ,  $A_2$   
and distinct eigenvectors  $V_1$  and  $V_2$   
associated with the eigenvalues.

But sometimes there is only one distinct eigenvector. An Example follows.

$$A = \begin{bmatrix} \alpha & i \end{bmatrix} \quad \text{Eigenvalues} \quad \lambda^2 - (\alpha + \alpha) \lambda + \alpha^2 = 0$$
  
$$\lambda_i = \alpha \cdot \lambda_2 = \alpha$$

$$V = \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} \implies \begin{bmatrix} a & 1 \\ 0 & a \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = a \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

$$= \int \left[ \begin{array}{c} av_1 + v_2 \\ av_2 \end{array} \right] = \left[ \begin{array}{c} av_1 \\ av_2 \end{array} \right] = \left[ \begin{array}{c} av_2 \\ av_2 \end{array} \right] = \left[ \begin{array}{c} av_2 \\ av_2 \end{array} \right] = \left[ \begin{array}{c} av_2 \\ av_2 \end{array} \right]$$

If we used our usual formula for the general solution for  $\dot{Y} = AY$ , we'd get the following:  $Y(t) = c_i V_i e^{at}$ .

How to find the graded solution?  

$$\hat{Y} = \begin{pmatrix} a & 1 \\ 0 & a \end{pmatrix}$$
  $\hat{y}_{1} = ay_{1} + y_{2}$   
 $\hat{y}_{2} = ay_{1} + y_{1}(0) e^{at}$   
 $\hat{y}_{1} = ay_{1} + y_{1}(0) e^{at}$   
 $\hat{y}_{1} = ay_{1} + y_{1}(0) e^{at}$   
 $\hat{y}_{1} = ay_{1} + y_{1}(0) e^{at}$   
Integrating (actor = e<sup>-at</sup> - Multiplying the above equality e<sup>-at</sup>;  
 $e^{-at}\hat{y}_{1} - ae^{-at}\hat{y}_{1} = y_{1}(0)$   
 $\frac{d}{dt}(e^{-at}\hat{y}_{1}) = y_{1}(0) \Rightarrow e^{-at}(y_{1} = y_{1}(0) + e_{1})$   
 $\frac{d}{dt}(e^{-at}\hat{y}_{1}) = y_{1}(0) \Rightarrow e^{-at}(y_{1}(0) + y_{1}(0))^{t}$   
 $\hat{y}_{1}(t) = e^{at}(y_{1}(0) + e^{-t}),$   
 $\hat{y}_{1}(t) = e^{at}(y_{1}(0) + y_{1}(0))^{t}$   
 $\hat{y}_{1}(t) = \hat{y}_{1}(0) + \hat{y}_{2}(0)$   
Frome portraid  $\hat{y}_{1}(t) = \frac{y_{1}(0)}{y_{1}(t)} = \frac{y_{1}(0)}{y_{1}(t)}$   
 $\hat{y}_{2}(t) = \frac{y_{1}(0)}{y_{1}(t)} = \frac{y_{1}(0)}{y_{1}(t)}$   
 $\hat{y}_{2}(t) = \hat{y}_{1}(0) + \hat{y}_{2}(0)^{t}$   
 $\hat{y}_{2}(t) = \hat{y}_{1}(0) + \hat{y}_{2}(0)^{t}$   
 $\hat{y}_{2}(t) = \hat{y}_{1}(0) + \hat{y}_{2}(0)^{t}$   
 $\hat{y}_{2}(t) = \hat{y}_{2}(0) + \hat{y}_{2}(t)^{t}$   
 $\hat{y}_{2}(t) = \hat{y}_{2}(t) + \hat{y}_{2}(t)^{t}$   
 $\hat{y}_{2}(t) = \hat{y}_{2}(t) + \hat{y}_{2}(t)^{t}$   
 $\hat{y}_{3}(t) = \hat{y}_{3}(t) + \hat{y}_{3}(t)^{t}$   
 $\hat{y}_{3}(t) = \hat{y}_{3}(t) + \hat$ 

NODE

Example 3

C70 and k70



Say- c2-4k<0 so that the eigenvalues are complex conjugates.  $\partial_{1,2} = -c \pm i \sqrt{4k - c^2} .$ general solution  $\chi(t) = e^{-\frac{c}{2}t} \left[ b_1 \cos \omega t + b_2 \sin \omega t \right]$ where was J4K-c2.





DRAWING THE PHASE PORTRAIT FOR NONLINEAR SYSTEMS

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Essentially the general way to draw the phone partrait for a montimear signters 
$$\dot{y} = f(y)$$
 is numerical - that is, solve the ODE for different initial conditions and plot  $y_i(t)$  is  $y_2(t)$ .

Let us consider an example: Simple pendulum with small 
$$c$$
.  
Equation:  $\ddot{0} + g \sin \theta + c \dot{\theta} = 0$ 

$$y_{1}=0$$
  $\dot{y}_{1}=y_{2}$   
 $y_{2}=0$   $\dot{y}_{2}=-k\sin y_{1}-cy_{2}$  where  $k=g/2$ .

LINEARIZATION AND LINEAR STABILITY

g .

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He have backed of this proposes  
At (0,0), the Stacobian matrix is 
$$\begin{bmatrix} 0 & 1 \\ -k & -c \end{bmatrix}$$
  
We know that the eigenvalues are  $\lambda_{1,2} = -c + \sqrt{c^2 - 4k}$   
For Sufficiently small c, three eigenvalues will be complex conjugate  
and the fixed point will be a STABLE SHEAL.  
At (T,0), the Jacobian matrix is  $\begin{bmatrix} 0 & 1 \\ k & -c \end{bmatrix}$   
The eigenvalues are  $\lambda_{1,2} = -c \pm \sqrt{c^2 + 4k}$ .  
 $\chi = -c$ ,  $\Delta = -k$ ,  $E^2 + 4\Delta > 0 = 2$  SADDLE POINT.  
 $\chi = -c$ ,  $\Delta = -k$ ,  $E^2 + 4\Delta > 0 = 2$  SADDLE POINT.  
 $\chi = -c$ ,  $\Delta = -1 + \sqrt{4} + 2$   
The eductor cogenerates let us reaks the parametric press.  
 $\chi = -2$   
Eigenvectors let us reaks the parametric press.  
 $\chi = -2$   
Eigenvectors are respectively  $\sqrt{42}$  and  $\binom{-0.4442}{0.8444}$   
 $(wing MANLAR)$ .  
 $\chi = -2$   
 $We TREELE DIRECTION$ 









PUTTING THE PICTURES TOGETHER.



So far so good. He can get a picture like about by following a sequence of well-defined steps.

But to complete the picture, we have no general technique that always works, except for computing the phase portroit. by bolving the ODE (say numerically). In this particular case, we can do a hitle better by appealing to physical intuition and knowledge of the nature of the solutions.

- If you start from the inverted position (±17,0) and give it on arbitrarily small perturbation, the pendulum oscillates and eventually comes to rest in the stately bottom position (0,0). In other words, the scalely points are connected to the

stable spiral.



GONNECTING THE SADDLES TO THE SPIRAL (THO DIFFERENT SPIRALS).



ADDING THE REST OF THE SADDLE.

Bifurcations (Intro/ Rough outline) Colloquially, à l'igurcation is a qualitative change in the dynamics of a system when some system parameter is changed. More formally, a bipurcation is said to have occured when the phase portrait's "topological structure" changes Recall from earlier when a parameter is varied. Example: change in the number and stability of fixed points.

The following are some of the most common bifurcations in 2D dynamics, very analogous to the corresponding 1D bifurcations.

In the following examples, you will notice that all the "bifurcation action" is happening along the x direction, whereas in the y direction, there is only simple stable dynamics.

Thus, it may superficially seem that these are 'special examples.'

But they are not really that special. Rather, they are called 'normal forms' or 'canonical forms'. Any other dynamical system having a similar bifurcation can be transformed, at least locally, into these normal forms using a continuous (often differentiable) transformation of variables. That is, these simple examples (normal forms) have the same topological structure of every such bifurcation (locally).

Bifurcations in 2D Saddle node:  $x = \mu - x^2$ y = -ySaddle a sodelle point and a rade come together and vanish as pe is varied across 120 (NOFPS) M=D .

 $\ddot{x} = \mu x - x^3 \quad \dot{y} = -y$ Supercritical pitchfork becomes pico (one stable node). puro. (2 stable nodes + 1 studdle point.) As It is change, one node becomes 3 FPs, two nodes + 1 soddle. Transcritical bifurcation Canonical example it = proc - x2, y = -y pro M20 two fixed points two fixed pts 2th = 0 - unstable xt = 0 - stable x\*= M70 stable xx = 14 < 0 - unstable x\* = o goes from statile to unstable Stable as pe is changed and at 150 the phase portrait is topologically different from when pro or prico. / unstable Honce this is a bipurcation. (even though the 120 and 1240 portrails look similar)

 $\bigcirc$ 

(How to know that FPI is unstable and FP2 and FP3 are stable? See end of this discussion on page 6.



4) The red line is other there are exactly 5 FPs. for K < redline slope (blockline) => 7 FPs. for k > redline slope (=) 3 FPs So just at the reduce slope ( a below it), 4 new FPs are created in 2 pairs - call then FP4 - FP7 as in previous page. - FP4 & FP6 are roughly located at +3.5TL when they are created. - FP6 & FP7 are roughly located at -1.5TL critical when created. red slope is roughly when K -> 0 KL 2.5T FP4 -> 311 > 41 FP5 -17 7 FP6 - 211 ' + SADDLE-NODE BIFURCATION FP7 > 41 31 FP3 20 1-01 ( soddle a vode oppeger obt of FPI T FP2 -SADDLE-NODE BIFURCATION. 9 this in) D\_ FP 7 - 211 - 311

As k is reduced even further a conother critical slope (shownin there arise 4 more fixed points, again in 2 pairs below). (one pair with 670 and another pair with 640).



So do FPIO and FPII. So extending the Bifurcation diagram a bit: Note that as k= 0 51 FP8 7 611 PP9 -> 6TT FPS FP10 -> -311 47 FP11 -> -411 FP3 27 FPI EP1 0 FP6

- 21

-411

As k is decreased further, we get more and more fixed points, all arising in pairs of saddle-node bifurcations. 6

Ok, how did we know what the stability of the fixed points whee?

$$\frac{FACT}{(You should be able to}; The fixed points ofshows this)} if the trian points of(Exercise). if the shows the trian the triangeneric ofare the some and thave the same staticity ofare the some as the fixed points and staticity ofbe + g rine + k(e-n) = 0So use can analyze the staticity of the 1D equation;be = k(n-e) - g rine = h(e) say-L h(e) > 0 ifh(e) > 0 ifh(e) > 0 ifh(e) > 0 h(e) > 0 h(e) > 0 h(e) > 0 ifh(e) > 0 h(e) > 0 h(e) > 0 h(e) > 0 h(e) > 0 ifg rine < k(n-e) + h(e) > 0 h(e) > 0 h(e) > 0 ifg rine < k(n-e) + h(e) > 0 h(e) > 0 h(e) > 0 ifg rine < k(n-e) + h(e) > 0 h(e) >$$

the fixed points are saddles, etc.