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# **Exploration-based learning of a stabilizing controller predicts locomotor adaptation**

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Humans adapt their locomotion seamlessly in response to changes in the body or the environment. It is unclear how such adaptation improves performance measures like energy consumption or symmetry while avoiding falling. Here, we model locomotor adaptation as interactions between a stabilizing controller that reacts quickly to perturbations and a reinforcement learner that gradually improves the controller's performance through local exploration and memory. This model predicts time-varying adaptation in many settings: walking on a split-belt treadmill (i.e. with both feet at different speeds), with asymmetric leg weights, or using exoskeletons – capturing learning and generalization phenomena in ten prior experiments and two model-guided experiments conducted here. The performance measure of energy minimization with a minor cost for asymmetry captures a broad range of phenomena and can act alongside other mechanisms such as reducing sensory prediction error. Such a model-based understanding of adaptation can guide rehabilitation and wearable robot control.

Humans readily adapt their locomotion to diverse environmental conditions and bodily changes<sup>1-3</sup> (Fig. 1a), but the computational principles underlying such adaptation are not fully understood. While crucial adaptation phenomena have been uncovered through careful experiments<sup>2-8</sup> and a handful of models have been proposed to explain individual experiments<sup>2,9,10</sup>, an integrative understanding of adaptation across paradigms and timescales is missing. Moreover, existing adaptation models are not implemented on a bipedal physics-based agent, and therefore do not encompass the stability-critical nature of adapting locomotion while avoiding falling. In this work, we put forth an integrative model of locomotor adaptation combining stabilizing control, performance-improving reinforcement learning, and performance-based memory updates. Our model predicts locomotor adaptation phenomena across paradigms in ten prior studies and two prospective experiments conducted in this study.

Theories of motor adaptation have predominantly been developed for discrete episodic tasks such as reaching with the arm<sup>11-13</sup>. Adaptation principles that explain such episodic tasks may not be sufficient for explaining continuously cascading stability-critical tasks such as locomotion, multi-fingered manipulation, and many activities of daily living. In episodic tasks like reaching where the arm's state is reset at the end of each episode, the errors during one episode do not dynamically propagate to the next episode. In contrast, in continuously cascading tasks like locomotion, errors can have short-term and long-term consequences to stability unless otherwise controlled<sup>14-17</sup>. Prior accounts of locomotor adaptation<sup>2,9,18</sup> do not consider the interaction with locomotor dynamics, perhaps assuming that dynamic stability is ensured by a distinct mechanism. For instance, metabolic energy reduction-based accounts<sup>2,19</sup> treated adaptation to be a univariate optimization process - implicitly assuming that changes on one step do not affect the next step through the dynamics. Similarly, error-based learning models developed for arm reaching<sup>11-13</sup>, when applied to locomotor adaptation<sup>9,10,18,20,21</sup>, do not usually interact with the locomotor dynamics; these models fit the kinematic symmetry error transients, without considering how these errors might affect stability. Here, we put forth a model that explains how humans adapt continuously during walking while maintaining dynamic stability.

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adapt readily to numerous locomotor task settings, both familiar and novel. **b** Description of the proposed hierarchical learning framework, containing three components: (i) the inner loop, represents a fast timescale response due to the stabilizing feedback controller (blue), aimed at avoiding falling; (ii) an outer loop, represents reinforcement learning (red) that tunes the parameters of the inner loop controller to improve some performance objective; (iii) storing and using memories of the learned controllers (green). Alternative adaptation mechanisms may include different performance objectives within the same framework (energy, symmetry, task error) or may replace the feedback controller by a sensorimotor transformation with a state estimator followed by the controller. These components act on the physics-based model of the human (Supplementary Fig. 1), allowing it to respond to perturbations and continuously adapt to new situations. **c** Reinforcement learning by mining exploratory noise to estimate gradient and improve the controller. Initially, the controller parameters  $p_1$  and  $p_2$  are near the optimum of the initial performance landscape (blue). When conditions change, the performance contours change (blue to orange) as does the optimum. Exploratory noise in the controller parameters, allows the learner to estimate the gradient of the performance objective and follow the negative of this gradient to improve performance. **d** Memory takes in task parameters and returns the stored controller parameters  $p_{memory}$  and the associated performance value  $J_{memory}$ . We describe how memory is used in concert with gradient-based learning. The control parameters  $p_i$  are updated toward memory  $p_{memory}$  when doing so improves performance (memory use); memory is updated toward the current parameters otherwise. Updates toward memory is degraded if these updates are not aligned with the gradient, and this degradation is mediated by a modified cosine tuning.

Improving some aspects of performance is a driving force for motor adaptation and learning. However, we do not understand which performance objectives explain diverse locomotor adaptation phenomena. Minimization of different types of error<sup>11,12,22-24</sup> (e.g., sensory prediction error, task error, proprioceptive conflict) or minimization of metabolic energy<sup>27,8,25</sup> have been separately posited as performance objectives underlying locomotor adaptation. However, these performance objectives often do not generalize across settings. Metabolic energy minimization can explain steady state adaptation in some experimental settings<sup>25,26</sup> but does not in other settings<sup>27</sup>. Similarly, while error-based learning models can be fit to asymmetry changes in some tasks<sup>3,4,6,10,18,24</sup>, they cannot make predictions for tasks where there is no changes in the symmetry<sup>28,29</sup>. A computational model that precisely specifies the performance objectives such as energy, sensory prediction error, proprioceptive conflict, etc. would help identify the performance objectives that predict locomotor adaptation phenomena across tasks. Here, we put forth such a predictive model of locomotor adaptation allowing comparisons between the predictive ability of different performance objectives, finding that energy minimization predicts the broadest range of phenomena.

In this work, we contribute a model of adaptation that causally links the body dynamics, stabilizing control policy, learning algorithm, performance goal, internal model of performance, and memory of control. We model adaptation as an exploration-driven gradient-based improvement of a stabilizing controller, explaining how humans improve their locomotor performance continuously while maintaining stability. Our model predicts adaptation phenomena in ten prior experimental studies and two model-guided experiments conducted here. The model captures learning phenomena such as fast timescale response followed by slow timescale adaptation, savings, faster deadaptation, generalization, non-learning in some situations, and the effect of noise and prior experience. By modifying the performance objective, we show that our modeling framework can help compare theories of locomotor adaptation such as minimizing energy, sensory prediction error (via proprioceptive realignment), or kinematic task error (e.g., asymmetry) in their ability to explain phenomena.

#### Results

#### A modular and hierarchical model of locomotor adaptation

We posit a modular and hierarchical model of locomotor adaptation (Fig. 1b–d) in which a controller keeps the human stable, a gradientbased reinforcement learner modifies this stabilizing controller to improve performance, an internal model learns to predict performance in a new environment, and a memory mechanism stores the improved walking strategies and deploys them when advantageous. The model is modular in that there are separate but interacting modules performing distinct tasks (stabilizing control, gradient estimation, gradient-based learning, memory update); the model is hierarchical in that some modules operate at and explain phenomena at distinct timescales that are hierarchically separated. We test the ability of the computational model to predict experimentally observed locomotor adaptation phenomena in a number of experiments: see our repository  $LocAd^{30}$  for the code implementing the model.

A critical constraint on human locomotion is being stable i.e. not falling down, despite internal and external perturbations. Thus, a stabilizing controller forms the inner-most level of our hierarchical model<sup>16,17,31</sup> (Fig. 1b), allowing the physics-based biped model (Supplementary Figs. 1, 2) to walk stably. We posit that during locomotion in a familiar setting, humans use a previously learned controller, which we call a 'default controller,' stored as a motor memory. We further posit that the structure of this default controller constrains how humans adapt to a novel situation. We characterized this default controller by modeling how humans respond to small deviations from nominal walking on the treadmill<sup>16,17,31</sup>. This controller can be decomposed into a feedforward component, not dependent on the biped's state, and other state-dependent feedback terms (see Methods). The same initial default controller can be used for all the locomotor adaptation tasks considered here (see Methods and Supplementary Methods) because the controller is robust to substantial noise and uncertainty as we have previously shown<sup>16,17</sup>, allowing the human to move stably in novel environments.

It has been hypothesized that the nervous system chooses movements that optimize some performance objective, for instance, reducing energy expenditure<sup>8,32–36</sup> or reducing left-right asymmetry<sup>3,18,24,37</sup> (Fig. 1b). We posit that when faced with a novel circumstance, humans gradually change their default stabilizing controller to optimize performance. This performance improvement is achieved through gradient-based reinforcement learning in an outer loop around the stabilizing controller (Fig. 1b, c). We found that allowing the reinforcement learner to adapt just the feedforward terms of the controller, leaving the stabilizing feedback gains unchanged, is sufficient to explain the observed phenomena. The learner estimates the gradient descent direction using 'intentional' exploratory noise<sup>2,13,38</sup> in the neighborhood of the default controller, contributing to increasing the step-to-step variability<sup>16,17,31</sup>. While the term 'reinforcement learning' has a multitude of algorithmic specifications<sup>39</sup>, here we use this term as shorthand for the proposed local explorationbased learning algorithm.

Motor adaptation involves memorization and retrieval of control policies. Here, we posit a module in the outer loop that forms longerterm motor memories<sup>40,41</sup> of the controllers being learned, parameterized by the settings in which they were learned. This stored memory is used when encountering a setting similar to one previously encountered (Fig. 1b, d), interpolating and generalizing between settings via function approximation<sup>39</sup>. Stored memory is only used when it may improve performance and does not conflict with gradient descent (Fig. 1d). Conversely, stored memory is updated when the current controller's performance is better than that of the motor memory. See *Methods* and the model's implementation in code, *LocAd*<sup>30</sup>, for further details.

We have posited that the gradual modification of a stabilizing controller for performance optimization is a primary mechanism for locomotor adaptation. Adaptation may also result from other mechanisms such as recalibration to reduce sensory prediction error<sup>11,22,42,43</sup>. Here, we extend the aforementioned framework, showing that the model can incorporate sensory error-based adaptation mechanisms, replacing the feedback controller of Fig. 1b by a more general sensorimotor transformation (see *Methods*).

## Predicting fast and slow timescale learning in many locomotor settings

The model predicted locomotor adaptation phenomena in many different conditions, including a split-belt treadmill, an asymmetrically added leg mass, external assistance, exoskeleton-based perturbations, and abrupt treadmill speed changes (Fig. 2). For the reinforcement learner, we tested minimizing four performance objectives: only energy expenditure, only asymmetry (specifically, step length asymmetry, defined below), a weighted sum of energy and asymmetry, and a kinematic task error. For the results below, we use energy expenditure alone or energy expenditure with a small step length asymmetry penalty as the performance objective as these give qualitatively similar results, we use the latter when the performance objective is not explicitly mentioned. The minimization of other objectives is discussed in their own separate sections later.

The most popular experimental paradigm used to investigate human locomotor adaptation is walking on a split-belt treadmill<sup>4,6,7,44</sup>, which has two side-by-side belts that can be run at different speeds. Most humans have never experienced this novel situation. Humans adapt to walking on a split-belt treadmill on the timescale of seconds, minutes, and hours, exhibiting stereotypical changes in their walking motion<sup>1,45,46</sup> and the model predicts these changes (Fig. 2a).

Specifically, within a few strides of split-belt walking, humans start walking with high negative step length asymmetry<sup>4,44</sup> – that is, the step length onto the slow belt is longer than the step length onto the fast belt (see Fig. 2a and Supplementary Fig. 1e). This is the fastest time-scale of adaptation, sometimes called early adaptation. This negative step length asymmetry becomes close to zero over a few hundred strides (about ten minutes), and then becomes slightly positive with more time<sup>7</sup>. The model predictions exhibit all these fast and slow transients both when minimizing just energy or energy plus a cost for

a) Model predictions vs experimental data: Fast and slow transients in split-belt walking predicted by model Split-belt speed protocol Model predicts step length asymmetry



b) Model predictions vs experimental data: Fast and slow transients while walking with an asymmetric foot mass predicted by model

Step time asymmetry transients Foot mass adaptation protocol Step length asymmetry transients Model prediction Expt data Model prediction Experimental data Added fraction foot mass added 0.2 0.05 0.2 step length asymmetry foot Data: Prentice Data: Prentice step time asymmetry mass Noble 2004 Noble 2004 eg with 0.12 0 added mass 0**⊾** -0.05 -0.2 2000 2000 Stride number 2000 0 0 Stride number Just Energy Energy+'symmetry

c) Model predictions vs experimental data: Step frequency in response to speed changes predicted by model Speed change protocol Step frequency in response to speed fluctuations



d) Model predictions vs experimental data: Walking with external assistance from an exoskeleton



**Fig. 2** | **Hierarchical model predicts locomotor adaptation in multiple task settings. a** Split-belt walking<sup>6,45</sup>, that is, with the two belts going at different speeds. Model qualitatively predicts experimental transients in step length asymmetry and metabolic energy during adaptation and de-adaptation. **b**. Walking with an additional mass on one foot<sup>5</sup>. Model qualitatively predicts experimental transients in step length asymmetry during adaptation and de-adaptation. Adaptation phases are shaded in blue in panels **a** and **b**. **c** Walking on a treadmill with abrupt speed changes every 90 seconds<sup>28</sup>. The model qualitatively predicts experimentally observed step frequency changes. Transients have a fast and slow timescale, with the fast timescale change sometimes undershooting and sometimes overshooting the steady state (red and green detail). Without learning, with just the feedback controller (gray), the fast transient is preserved but the slow transient is replaced by a (noisy) constant. **d-i** Walking with an exoskeleton that provides periodic propulsive impulses<sup>48</sup>. **d-ii** Stride period converges to the perturbation period, implying entrainment. Different trajectories starting from different initial conditions are shown. **d-iii** The perturbation phase converges to zero (heel-strike) in both model predictions and experiments. Different model trajectories show trials starting from different initial conditions. All quantities are non-dimensional.

step length asymmetry (Fig. 2a). The model predicts an immediate initial increase in energy cost upon encountering the split-belt condition, which then reduces to a lower steady state gradually, as found in prior experiments<sup>6</sup>. When the split-belt condition is removed, the model predicts a fast-timescale transient to large positive step length asymmetry (a learning after-effect) and then a slow de-adaptation back to normal walking. The model predicts this de-adaptation to be faster

than the adaptation, as found in experiments<sup>4,7,44</sup> (Fig. 2a). The model also predicts that a steady state is reached more quickly for step time asymmetry, and that the energy cost is more sensitive to step time asymmetry compared to step length asymmetry (Supplementary Fig. 3), as suggested by some prior experiments<sup>6,47</sup>.

Human adaptation proceeds analogously when they are made to walk with an extra mass attached asymmetrically to just one ankle, as characterized by a prior experiment<sup>5</sup>. The model predicts the qualitative features of such adaptation, whether the performance objective is just energy or has an additional symmetry term (Fig. 2b). In both experiments<sup>5</sup> and in our model, the walking gait becomes asymmetric in step length and then, during slow timescale adaptation, gradually tends toward symmetry; when the extra mass is removed, the asymmetry jumps to the opposite side, and then gradually de-adapts to normal walking.

The model predicts the step frequency changes while walking at varying speeds on a 'tied-belt' treadmill – which is just a regular treadmill with one belt, or equivalently, a split-belt treadmill with equal belt speeds (Fig. 2c). In prior experiments<sup>28</sup> in which the belt speed was changed every 90 seconds, humans quickly adapt their step frequency within 2 seconds and then slightly adjust their step frequency over a longer timescale – with the initial fast transient either overshooting or undershooting the ultimate steady-state frequency slightly. In previous work<sup>28</sup>, the overshooting and undershooting transients required separate fits, whereas our model predicts both with the same framework.

The model captures empirical findings of how humans adapt to exoskeleton assistance. In some prior experiments<sup>29,48</sup>, humans were provided with time-periodic ankle torque impulses via a robotic exoskeleton (Fig. 2d). If the time period of these external impulses was close to the human stride period and the impulse magnitude was in the right range, individuals changed their stride frequency to entrain to this external impulse frequency, as predicted by the model (Fig. 2d-ii). Both model and experiment show entrainment that approximately aligns the external impulse with the transition from one step to the next (Fig. 2d-iii). The model can show entrainment whether the external impulse frequency is faster or slower than the stride frequency<sup>29,48,49</sup>, as found in prior experiments, while prior modeling work has captured entrainment for higher frequencies only with feedback control and without learning<sup>29</sup>. As in prior experiments<sup>29,48</sup>, the model does not entrain on every trial but only on some fraction of the trials. Rather than provide such time-periodic assistance, if the external assistive forces from the exoskeleton are a simple function of the current body state (and not too noisy), the learner predicts successful adaptation toward the new performance optimum (Supplementary Fig. 4). We consider other such exoskeleton adaptation studies later in this manuscript.

#### Lesions in simulation identify modules responsible for the fast and slow adaptation transients

We can analyze which hypothesized modules in the model are responsible for explaining specific observations by the computational analog of 'lesion experiments': that is, turning off specific modules and noting what experimentally observed adaptation feature is degraded or lost. The following observations apply to all but the exoskeletal entrainment of the previous section, but we center the discussion on split-belt walking.

Turning off the default stabilizing controller by setting all feedback gains to zero often makes the biped fall to the ground when the novel condition is initiated. Lowering the feedback gains to near zero results in falling or degraded learning (Fig. 3a, b) in the presence of sensory noise. Thus, the stabilizing controller is critical for effective locomotor adaptation. Further, this exercise of lowering the feedback gains closer to zero leaves a large fraction of the initial transients intact (Fig. 3a).

The fastest transient (early adaptation i.e., the initial response immediately upon experiencing the new condition) is entirely due to the default controller and the natural dynamics of the biped. Turning off both the reinforcement learner and the memory mechanism still results in the fast timescale initial response due to the stabilizing controller (Fig. 4a). Recent experiments partially corroborate this prediction, showing that providing gait stability through other means (e.g., handrail) affects this initial transient<sup>50,51</sup>, though such experiments may have changed other aspects of the gait than just stability.

The slow adaptation transient when first exposed to the novel condition is due to the reinforcement learner improving performance. Turning off the reinforcement learner and the memory mechanism with zero learning rates results in the fast timescale initial response due to the stabilizing controller (Fig. 4a), but no slow timescale adaptation response. Thus, the stabilizing controller alone cannot explain the slow transients. Turning on the reinforcement learner results in a slow timescale adaptation response. Changing the learning rate for the reinforcement learner modulates the speed of this slow adaptation (Fig. 4b). In the first exposure to these novel situations, there is not yet any memory to call upon, and therefore, memory specific to the novel situation does not contribute to the first adaptation.

De-adapting to a familiar situation (equal belt speeds) after exposure to a novel situation will involve the use of stored memory of the familiar situation. Specifically, in split-belt walking, our model predicts that the de-adaptation will be faster than adaptation due to the use of stored motor memory of walking with tied-belts (Fig. 2a)<sup>6,45</sup>. Turning off this memory use, the de-adaptation is slower than adaptation (Fig. 4c). During the first adaptation to a novel setting, the slow transients are governed by gradient descent, whereas during de-adaptation back to a familiar setting, the slow transients are sped up due to the summing of gradient descent and progress toward stored memory (Fig. 1d).

#### Explaining savings, generalization, and anterograde noninterference

'Savings' refers to the faster re-learning of a task that has previously been experienced. In prior experimental work, such faster re-learning during a second split-belt adaptation experience was observed<sup>1,52</sup>, despite having a prolonged tied-belt period between the two adaptation periods (Fig. 5) – this intervening tied-belt period allows for full 'washout', complete de-adaptation in terms of observable variables. Here, our model qualitatively predicts such empirically observed savings (see Fig. 5 and Supplementary Table 1 for statistics). Such faster relearning in the model is due to the motor memory mechanism, which stores how the controller changes under different situations. Motor memories are formed during first exposure to a novel condition, and then when exposed to this condition again, the re-learning is faster due to gradient descent and memory use acting synergistically (Fig. 1d). Because the motor memories are task-dependent, memories for splitbelt adaptation do not decay entirely during tied-belt washout as the two tasks are non-overlapping. This persistent memory from the first exposure to split-belt walking results in the observed savings.

'Generalization' is when adaptation under one task condition results in savings or faster adaptation for a different task condition. Humans exhibit generalization during locomotor adaptation and our model predicts this phenomenon (Supplementary Fig. 5a, b). Specifically, in one prior experiment<sup>53</sup>, humans exposed to a split-belt trial A showed savings for a split-belt trial B with a smaller speed difference between both belts than A. Thus, experience with task A sped up adaptation to task B, suggesting that humans generalized from A to B. Further, it was observed<sup>53</sup> that such savings for task B from experiencing task A (with the larger belt-speed difference) were higher than the savings obtained if the first adaptation experience was with task B instead. Our model predicts both these generalization phenomena (Supplementary Fig. 5a, b) due to the motor memory being continuously parameterized with respect to continuous-valued task parameters (here, belt speeds), so that the controller for intermediate conditions is interpolated even if they are never directly encountered. Such generalization cannot be predicted by models in which memories are stored discretely without interpolation<sup>2</sup>.

'Anterograde interference' is when adapting to one task makes you worse at adapting to the 'opposite' task: opposite locomotor adaptation tasks could be split-belt walking tasks with belt speeds Significance of the stabilizing feedback controller: avoiding falling and improving learning

a) Lower feedback gains results in much lower adaptation and greater gait variability



despite noise and environmental changes. Substantially lowering the feedback gains, all by the same factor, reduces the effective adaptation rate and increases gait variability. The sensory noise in these simulations is fixed across these feedback gain conditions and is added to velocity feedback to the feedback controller. Adaptation phases are shaded in blue. b Lowering the feedback gains even further results in falling of the biped upon introducing the split-belt perturbation. Three

asymmetric gait, and split-belt walking with much-reduced feedback gains resulting in falling. In the bottom-most row, the center of mass trajectories for each stance phase are shown relative to the respective stance belt frame for visualization purposes (so that the split-belt trajectories for the different stance phases are with respect to different frames).

switched. Contrary to arm reaching adaptation studies where such anterograde interference is observed<sup>41</sup>, our model predicts that such interference need not happen in locomotion: that is, adapting to one perturbation need not make you worse at adapting to the 'opposite' perturbation if there is a sufficient tied-belt washout period between the two adaptation phases (Fig. 6a). This non-interference can be explained by the memory mechanism incorporating a function approximation, so that it can meaningfully extrapolate the learned controllers to the opposite perturbation as well. Such non-interference was indeed found in prior locomotor experiments<sup>52</sup>.

To further test the model's predictions on how prior experience shapes adaptation, we performed prospective experiments here: we tested adaptation to two opposite split-belt tasks A and B without a washout period (see Fig. 6b), while prior experiments had a substantial assistance

Exokeleton assistance

-0.1

0.6

High release

toward optimum

See Selinger et al 2015

Exo on

3000

Adaptation

for Experiment

2000

Step number



Energy without exo

0.9

Step frequency

1.1

0.9

0.7

0

No adaptation

Step number

toward optimum

1000

Step frequency

Fig. 4 | Effect of learning rate, memory and sensory noise: Model captures degraded learning, non-learning, and improving with guided experience.
a Stabilizing feedback controller alone only captures the fast learning transient. Addition of the reinforcement learner is needed to capture the slow transients.
b Increasing the learning rate parameter speeds up learning (for a range of learning rates). c Progress toward memory makes de-adaptation faster than adaptation.
d Increasing sensory noise degrades learning for fixed learning rate and fixed exploratory noise, resulting in less learning and less energy reduction. Split-belt adaptation phases are denoted by green shaded region in panels a-d. e Model captures experimental phenomena<sup>2,8</sup> wherein a human does not adapt to an

normal

step frequenc

0.9

Step frequency

0.18

0.12

0.06

0.6

Optimum

with exo

Metabolic rate

exoskeleton that provides step-frequency-dependent assistance upon the first encounter, but adapts toward the energy optimal frequency when provided with broad experience across a range of frequencies via a metronome-tracking condition. On the right two panels, blue indicates baseline condition without any assistance, red indicates exoskeleton assistance condition, and green indicates metronome-tracking condition in addition to exoskeleton assistance. In the rightmost panels, the `exo on' condition (red) shows no adaptation before the broad experience (green), but shows adaptation after the broad experience. All quantities are non-dimensional.

0

Baseline (exo off and no metronome)

Metronome on and exo on

1000

washout period between the split-belt phases<sup>52</sup>. We found that the model predicted both the increased initial step length asymmetry transient due to the recent adaptation to the opposite task and the insignificant changes to adaptation time-constants (see Fig. 6b and Supplementary Table 1 for comparisons and statistics).

More generally, our model qualitatively captures the effects of different split-belt adaptation protocols, for instance, capturing the time course of step length asymmetry when the split-belt phase is introduced gradually or abruptly, and whether these adaptation phases are short or extended<sup>18,20</sup> (Supplementary Fig. 6). Having a longer duration adaptation phase in which the perturbation grows gradually may sometimes result in less savings than a shorter adaptation phase in which the perturbation began abruptly and remains constant (Supplementary Fig. 6). In previous work, an explicit memory of errors was

used to explain some of these results<sup>9</sup>, but we have provided an alternative explanation via different model assumptions. In these cases (Supplementary Fig. 6), we found that the adaptation to different kinds of exposure to gradual and abrupt conditions can depend on protocol-specific parameters (e.g., duration of different phases, perturbation magnitude, learning rates); this suggests that one must be cautious of claiming general trends based on limited experiments.

The model predicts how the size and duration of perturbations affects adaptation<sup>1,18,53</sup>. In split-belt walking, both in the model and in prior experiment<sup>53</sup>, being exposed to a larger belt-speed split results in larger initial transients and more positive final asymmetry (Supplementary Fig. 5c). Being exposed to a condition for a shorter period of time results in smaller savings than being exposed to the condition for longer<sup>18</sup> (Supplementary Fig. 6).



**Fig. 5** | **Savings.** `Savings' refers to the phenomenon that humans re-adapt faster to a condition (say, split-belt walking) if they have experienced the condition before, even if they have fully de-adapted to normal walking in the intervening time. **a** A treadmill protocol with two split-belt adaptation periods with an intervening tiedbelt washout de-adaptation phase (W) that brings all the externally observable state variables as well as the current controller back to baseline – but not the internal memory state, which remembers the past learning. First adaptation (blue shaded region) and re-adaptation (red shaded region) transients are shown. **b** The model

## Degraded learning, non-learning, and making non-learners adapt via experience

The human motor system has sensory noise and motor noise that is not fully observable, and is thus distinct from intentional exploratory noise. The results presented thus far were obtained with low levels of sensorimotor noise. When the sensorimotor noise is less than a critical threshold, it preserves the qualitative results despite degrading the gradient approximation and thus degrading the effective learning rate (Fig. 4d). Large enough sensorimotor noise for fixed exploratory noise destroys the reinforcement learning entirely, resulting in no kinematic adaptation or energy reduction upon first exposure (Fig. 4d), potentially explaining why some populations with movement disorders may have impaired learning<sup>54</sup>.

Prior adaptation experiments involving exoskeleton assistance found that some humans were able to adapt spontaneously whereas others did not<sup>2,8,27</sup>. The non-spontaneous learners, when exposed to broad experience with a lower associated metabolic cost, were able to adapt toward the energy optimum<sup>2,8</sup>. In our model, both spontaneous learning and non-learning was possible depending on the size of sensorimotor noise: low noise resulted in spontaneous learning and high noise resulted in non-learning. As in experiment<sup>2,8</sup>, the model's nonlearners could be made to adapt toward a lower energy cost by giving them broad experience on the energy landscape, giving them experience of a lower energy cost to be stored in memory (Fig. 4e). In our model, this adaptation upon providing experience stems from motor memory formation and later memory use in addition to improving performance through gradient descent.

In addition to intrinsic sensorimotor noise, adaptation to external devices such as exoskeletons or treadmills could also be degraded by 'device noise'. Our model predicts that split-belt adaptation can be degraded via such device noise when implemented as noisy belt speed fluctuations that are large enough (Fig. 7a). To test this model prediction prospectively, we performed human experiments and compared the post-adaptation after-effects of noise-free and noisy splitbelt protocols. We found that participants had lower after-effects after the noisy adaptation condition, as predicted by the model; see Fig. 7a and Supplementary Table 1. This device-noise-based degradation may seem in conflict with earlier experiments by Torres-Oviedo and Bastian<sup>20</sup>, who compared adaptation in a split-belt protocol under noise-free and noisy belt speed conditions and found that the noisy version had higher adaptation as judged by the post-adaptation aftereffects. However, our model also captures this improved adaptation due to a different implementation of device noise in this prior experiment<sup>20</sup> by incorporating that specific experimental protocol in with memory predicts this experimentally observed savings phenomenon<sup>52</sup>. Step length asymmetry changes are faster during re-adaptation compared to the first adaptation. The re-adaptation has a smaller initial transient compared to the first adaptation. The time-constants of first adaptation and re-adaptation are computed by fitting a single exponential to the step length asymmetry transients, showing that re-adaptation has a faster time-constant. See Supplementary Table 1 for statistical details of comparisons. All box-plots show the median (red bar), 25–75% percentile (box), non-outlier range (whiskers), and individual data points (pink circles).

the model (Fig. 7b), thus reconciling the seemingly conflicting findings. These results illustrate that the details of the noise pattern (e.g., magnitude and temporal correlations, see *Methods*) and the adaptation protocol used are important to determine the impact of device noise on adaptation, i.e., there are many ways to add device noise and some may enhance learning and others may degrade it.

Aside from noise-based explanations, we provide one more potential cause for initial non-learning observed in some exoskeleton studies: delay between human action and exoskeleton response. Many exoskeleton adaptation experiments in which participants did not spontaneously adapt<sup>2,8,27</sup> had an exoskeleton controller that provided assistance or resistance based on the participant's previous walking step, resulting in a delay between action and energetic consequence. We showed that such delays can degrade or even stop gradient descent-based learning (Supplementary Fig. 7), making adaptation not obligatory. The gradient estimate is degraded due to poor credit assignment: when there is a delay, the reinforcement learner in our model associates the effect with an incorrect cause, as the learner's inductive bias assumes no such delays.

## Alternative to energy minimization: Comparing to minimizing asymmetry

To explain split-belt adaptation, researchers have treated the left-right asymmetry in step length as the error being corrected, fitting equations with one or two time constants to describe the observed decrease in this asymmetry<sup>1,9,10</sup>. Here, we examined what predictions our model makes if step length asymmetry is used in our optimization framework as the only performance objective, a variant of another study<sup>24</sup> in which foot contact time symmetry was optimized. We find that minimizing asymmetry does not fully capture the slow timescale transients in either tied-belt or split-belt locomotion. First, for changing treadmill speeds during tied-belt locomotion<sup>28</sup>, minimizing asymmetry predicts the fast timescale changes in step frequency due to the default controller, but further slow timescale changes observed in experiment are not predicted by an asymmetry-minimizing objective alone. During split-belt adaptation, while minimizing just step length asymmetry, our model predicts convergence to pure step length symmetry (Fig. 8a). This is in contrast to recent experiments which suggest eventual convergence to positive step length asymmetry<sup>45</sup>. In general, minimizing asymmetry is insufficient as the lone performance objective in an optimization framework, as perfect symmetry admits infinitely many locomotion patterns<sup>55</sup> and does not result in isolated local minima required for stereotypy. Thus, minimizing asymmetry alone cannot predict the many steady-state

Two experiments for testing `interference'

a) Model predicts no significant interference when comparing the final 'A' in the protocols T-A-T-A and T-A-T-B-T-A (as in Malone and Bastian, 2011)

Model predictions: No significant difference in first step or early change with or without the counter perturbation



b) Model predicts behavior in new experiments comparing adaptation A and B-A Comparing two adaptation protocols No significant difference in adaptation rate constant



Initial response is significantly higher immediately after prior experience with a counter perturbation (without washout) Model predictions Experimental results Experimental time-series data



**Fig. 6 | Interference.** `Anterograde interference' refers to the phenomenon where humans sometimes adapt slower to a condition A when they were previously exposed to the opposite condition B, that is, with the belt speed differences reversed between the two belts. **a** We performed simulations of two split-belt adaptation protocols: first, T-A-T-A, alternating between tied-belt conditions T and the split-belt condition A, and second, T-A-T-A, where one of the A phases is replaced with the opposite condition B. We compare the adaptation between the two protocols during the final A phase (denoted as yellow shaded region). We find that the two protocols are not significantly different in their initial response to the perturbation or the early change in the step length asymmetry for the final adaptation period (yellow shaded region), as shown by Malone et al<sup>52</sup>. **b** To test if this non-interference remains in the absence of washout, we performed prospective experiments in the absence of such a tied-belt washout phase: we compared

protocols T-A with T-B-A with both simulations and human participant experiments. In experiments, we found that the initial step length asymmetry (first step of A) was significantly higher when B was present and the time constant of adaptation during A was not significantly different under the two conditions. This confirmed our model simulations, which predicted that the initial transients for A will be higher after B. The model also predicted no statistically significant difference in the adaptation rate constant in the presence of inter-participant variability of magnitude similar to that in the experiment. All box-plots show the median (red bar), 25–75% percentile (box), non-outlier range (whiskers), and individual data points (pink circles). The time-series shows median as thick colored line and light gray lines are individual participant data overlaid. See Supplementary Table 1 for statistical details of comparisons.

locomotor phenomena predicted by minimizing energy during normal locomotion<sup>28,33,56</sup>. As a corollary, when placed in any symmetric situation with a symmetric body (e.g., slopes or bilaterally symmetric exoskeletons), minimizing asymmetry will result in zero slow timescale

adaptation of the controller even if the mechanical environment is changed substantially, in contrast to experimental findings<sup>2,8,27</sup>. While minimizing asymmetry alone does not explain diverse locomotor phenomena, minimizing a heuristically weighted combination of

#### Effect of environmental noise on learning

Model predicts non-monotonic effect of belt noise on split belt walking, confirmed by experiment a) Noise can degrade adaptation after-effects (comparison with new data from the present study)



b) Noise can improve adaptation after-effects (Comparison with data from Torres-Oviedo and Bastian, 2012) 'Gradual Noisy' and 'Abrupt No Noise' protocols produce larger



**Fig. 7** | **Split-belt learning can be degraded or enhanced depending on noise structure. a** Split-belt adaptation with and without belt-noise are compared. Adaptation phases are shaded in light green. The speed fluctuations in the noisy split-belt condition are continuous and piecewise linear and happen roughly every step. Model predicts that when the belt noise is high enough, adaptation can be degraded, as judged by lower post-adaptation after-effects. The post-adaptation after-effects shown are the initial step length asymmetry when the tied-belt condition starts after the split-belt adaptation. We performed model-guided prospective human experiments that confirmed these predictions: *p* value showing

significant difference is from one-tailed t-test (unpaired, t(df) = -2.41(14), p = 0.0151). **b** Torres-Oviedo and Bastian<sup>20</sup> found that appropriately structured noise accompanied by gradual speed change can enhance adaptation, as measured by post-adaptation after-effects: box plot with these prior experimental results<sup>20</sup> shows mean (red line) and standard error (box). Our model captures this behavior. All box-plots show the median (red bar), 25–75% percentile (box), non-outlier range (whiskers), and individual data points (pink circles). See Supplementary Table 1 for full statistical details of comparisons.

energy and asymmetry, with a small weight on the asymmetry, retains the qualitative predictions of minimizing energy, while sometimes allowing a better quantitative match (Figs. 2a–b and 8a). Future experiments could delineate the extent to which humans have symmetry as an explicit objective in addition to energy<sup>57</sup>, given that energy<sup>55</sup> and other performance objectives such as proprioceptive realignment (as shown below) may also indirectly promote symmetry<sup>22,42</sup>.

## Alternative to energy minimization: Comparing to minimizing generalized task error

In low-dimensional adaptation tasks such as reaching with the arm to a target, the task error to be minimized is unambiguous; for instance, in reaching tasks with visuomotor rotation, the error is defined as the angular distance to the reach target<sup>9,12</sup>. However, in higherdimensional tasks like locomotion, analogous definitions of task error as deviation from desired body kinematics is not uniquely defined: for instance, the total task error could be defined as a weighted sum of the error from desired body states, with errors for different states weighted differently – but such a weighting would not be uniquely specified. Here, we considered a few such relative weightings and made model predictions for minimizing such kinematic task errors as the only performance objective (see *Methods* and Fig. 8b) via the exploration-driven gradient descent of Fig. 1b.

The resulting predictions were not entirely consistent with the experiment. Different relative weightings resulted in distinct behaviors, all of which fell short of fully capturing the experimental findings: the weighting that results in eventual positive step length asymmetry, as seen in experiment, corresponded to energy increase in contrast to experiments, and on the other hand, the weighting that results in monotonic energy decrease has a steady state with substantial negative step length asymmetry, again in contrast to experiments (Fig. 8c). A purely kinematic performance objective was similarly found to not explain exoskeleton adaptation in prior experiments, where participants achieved entrainment to exoskeleton impulses<sup>48</sup> or changed their walking frequency<sup>8</sup> without plateauing at the unassisted walking kinematics.

## Alternative to performance optimization: Comparison with proprioceptive realignment

Proprioceptive realignment has been proposed as a potential mechanism accounting for the adaptation seen in split-belt locomotion<sup>22,42</sup> and for arm-reaching tasks with visuomotor perturbations<sup>58,59</sup>. Vasquez et al<sup>42</sup> characterized the (proprioceptively) perceived speed of the legs after a split-belt adaptation, effectively



**matic task error. a** As an alternative to an energy objective, minimizing asymmetry of nine asymmetry as the only objective during split-belt adaptation results in a perfectly symmetric gait in the model, which conflicts with the positive step length asymmetry found in experiment as well as when predicted by an energy minimization<sup>45</sup>. **b** As another alternative to an energy objective, we formalize the minimization of kinematic task error as minimizing deviation from preferred walking kinematics defined for each speed. A single common belt speed is estimated by a state estimator using sensed body speeds relative to the lab and the belt (vision and proprioception). The task error is deviation from kinematics at that estimated speed

under tied-belt conditions, drawn from memory. **c** Model predictions for minimizing just task error without an energy objective; two different weightings are used for different components of the kinematic error (red and yellow). Energy minimization is shown for comparison (blue). For the task error predictions, one of either step length asymmetry or energy trends disagree with split belt adaptation experiments<sup>45</sup>: either the step length asymmetry stops well short of symmetry while decreasing energy somewhat (yellow), or the energy transients are not monotonically decreasing (red). Light green shaded region in all panels is the period of split-belt adaption.

finding that humans perceived the fast leg as being systematically slower than reality or the slow leg as faster than reality or both. A causal mechanism relating this sensory recalibration to locomotor adaptation has not previously been proposed, and a mathematical model could help establish if proprioceptive realignment could result in symmetry changes consistent with the experiment.

We put forth a mathematical model of proprioceptive realignment via sensory recalibration using our framework, which enables linking body dynamics, sensory feedback (both proprioception and vision), and motor action. In our model, we posit that the nervous system expects the two legs to be on the same walking surface and proprioceptive deviations from this sensory prediction are perceived as an error to be corrected by recalibrating proprioception; while only proprioception is recalibrated, vision is used as a common sensory signal to estimate the proprioceptive conflict between the two legs (see *Methods* and Fig. 9a). This is a type of sensory prediction error<sup>12,59</sup>, as it is due to a difference between the sensory feedback and what the nervous system expects. This model results in recalibrated estimates of leg speeds such that on a split-belt treadmill, the fast leg feels slower and the slow leg feels faster than reality, as in experiment<sup>42</sup> (Fig. 9c), with the recalibration growing in time. The model produces no recalibration when walking on a tied-belt, as in experiment<sup>42</sup>. We incorporated this recalibrating proprioceptive sensing as a feedback input to the stabilizing controller without changing other aspects of the default controller to predict what proprioceptive realignment alone can predict.

Proprioceptive realignment as implemented here falls short of explaining the qualitative features of split-belt locomotor adaptation. Specifically, while the initial negative step length asymmetry produced by the default controller is decreased by proprioceptive realignment, the steady state of the adaptation still has substantial negative asymmetry (Fig. 9d), falling substantially short of experimentally observed symmetry<sup>6,60</sup> and positive step length asymmetry<sup>7,45</sup>, which is predicted by energy optimization. Interestingly, the model shows coincidental metabolic energy decrease as a result of proprioceptive realignment (Fig. 9e), but this energy decrease is not accompanied by kinematic changes observed in experiment. Thus, while proprioceptive realignment could potentially be a partial cause of split-belt adaptation, it does not explain all the associated adaptation phenomena, as also suggested by recent experiments<sup>61</sup>. Beyond split-belt adaptation, proprioceptive realignment cannot explain how humans respond to tied-belt speed changes<sup>28</sup>, as experiments did not find

## Alternative to minimizing energy: Sensory recalibration for proprioceptive realignment

a) Sensory recalibration

Split-belt can cause sensory conflict Sensory conflict leads to sensory recalibration: Model of sensory recalibration



b) Replacing the feedback controller by a sensorimotor transformation that includes sensory recalibration



c) Proprioceptive realignment due to sensory recalibration



d) Model predictions: Proprioceptive realignment reduces step length asymmetry but falls short of symmetry





e) Model predictions: Proprioceptive realignment coincidentally reduces energy even when energy is not the optimized objective



• 50% sensory recalibration (as in experiment)

100% sensory recalibration

Energy minimization



proprioceptive estimate to obtain the recalibrated proprioception. The correction for the fast leg is positive and that for the slow leg is negative. 100% recalibration corresponds to completed proprioceptive realignment and 50% recalibration is close to that observed in experiment<sup>42</sup>. **d** Using the recalibrated proprioception as feedback in the stabilizing controller results in the reduction of step length asymmetry, but even 100% recalibration does not result in symmetry or positive step length asymmetry. Thus, the model predicts that proprioceptive realignment cannot be fully responsible for split-belt adaptation. **e** Proprioceptive realignment also reduces energy coincidentally even without energy being an explicit objective in this situation. Light blue shaded region in panels c-e is the period of split-belt adaption.

significant proprioceptive realignment in the tied-belt condition<sup>42</sup>. Finally, proprioceptive realignment via interaction with vision, as implemented here, cannot explain adaptation to purely mechanical changes to the body or the environment such as an added mass or an exoskeleton.

#### Interaction with explicit feedback

Our framework is meant to model implicit adaptation and learning, but can accommodate explicit adaptation mechanisms acting in parallel. One potential way to speed up locomotor adaptation is to provide explicit verbal instruction to the participant about the desired behavior or provide visual feedback on the error between desired and actual behavior<sup>10</sup> (Fig. 10a). Indeed, providing visual feedback on step length asymmetry to participants on a split-belt treadmill and asking them to reduce this asymmetry hastened the progress toward symmetry – compared to adaptation without this feedback<sup>10</sup>. Removing this visual feedback partway through adaptation results in the increased symmetry being largely wiped out, so that the asymmetry



are compared. Protocol 0 which is a typical split-belt protocol with no explicit feedback about step length asymmetry. In protocols 1 and 2, participants are shown visual feedback of step length asymmetry on a screen and asked to reduce it explicitly, either partly through the adaptation phase (protocol 1) or partly through the de-adaptation phase (protocol 2), **b** Explicit control is modeled as a module that adds to the nominal step length of the `implicit controller' and this correction is

proportional to the step length asymmetry on the previous step. The explicit and implicit modules are in parallel, and the implicit learner only knows about the motor command from the implicit feedback controller that it tunes. Having the explicit feedback improves progress to symmetry during c adaptation and d deadaptation but this symmetry improvement is lost when the explicit feedback is removed, as found in experiment<sup>10</sup>.

goes back approximately to where it would have been without the explicit feedback. We were able to capture this phenomenon (Fig. 10c, d) by adding a separate module for explicit control that acts in parallel to the feedback controller in memory (Fig. 10a), as hypothesized in some prior work<sup>10,23</sup>. This demonstration is mainly to show that the implicit learner of Fig. 1b can be readily modified to accommodate explicit mechanisms without degrading the implicit learner's performance. This demonstration also shows that kinematic behavior changes due to explicit corrections need not, by themselves, be sufficient to modify implicit learning, as seen in experiments<sup>10,21</sup>.

#### Discussion

We have presented a model for locomotor adaptation that captures observed experimental phenomena in ten different studies<sup>3-8,18,20,28,48,52,53</sup>, and predicts phenomena observed in two prospective experiments conducted in this study. Across these studies, our model captures adaptation transients in both the short timescale of seconds and the long timescale of many tens of minutes. Our model also enabled us to compare different adaptation mechanisms, specifically energy optimization via reinforcement learning, proprioceptive realignment, and reducing sensory prediction error<sup>22,42,59,62</sup>, delineating how the hypotheses differ or coincide in their predictions and allowing testing through future prospective experiments. We have shown how

humans could adapt to perturbations to the body or the environment while walking stably and continuously without falling or stopping, as models of non-continuous episodic tasks such as arm reaching do not show how this is possible.

Predictive models of motor learning such as the one proposed here could be used to improve motor learning in the real world. We have made predictions about conditions that may degrade or accelerate learning consistent with prior experiments. Given this, future hypotheses for improving learning could be tested computationally within our modeling framework before testing via prospective experiments. We have tested the model by performing two such prospective experiments here, one for examining anterograde interference and another for the effect belt noise. Further, such experiments may either provide further evidence supporting the model or information that could help improve the model. If the goal is to improve learning to use a device (such an exoskeleton or a treadmill), the device parameters and their sequencing can be optimized in simulation to reduce the time duration to learning steady state.

Our model suggests explanations for why humans may adapt reliably in some novel situations (for instance, during split-belt walking  $^{4,6,20}$ ) and not others (for instance, some exoskeleton studies<sup>2,8,19,63</sup>). One might wonder if common principles underlie such reliable adaptation in one class of devices and unreliable adaptation in

another class, which is plausible given that both devices are interacting with the same human motor control system. First, we note that both exoskeletons and split-belt treadmills share a core dynamical similarity: they are both mechanical devices that contact the body, applying forces and performing positive or negative work of different specifications<sup>45</sup>. Second, our results also suggest that the two classes of devices are not fundamentally different with respect to motor learning. Our model suggests ways in which we can make participants less reliable learners on split-belt treadmills and reliable learners on exoskeletons and prostheses. Specifically, our model predicts that split-belt adaptation can be degraded by noisy belt speed variations (Fig. 7) which we confirmed with our prospective experiment. We also noted that many exoskeleton studies that did not show obligatory adaptation involved exoskeleton controllers that had a one-step delay between human action and the device response<sup>2,8,19</sup>. We showed that gradient descent can be degraded or entirely stopped in the presence of such delays (Supplementary Fig. 7), whereas there can be reliable learning in exoskeletons with no delay or noise (Supplementary Fig. 4); this prediction can be tested by systematically manipulating the device delay in future experiments. In summary, we suggest that humans may exhibit better adaptation to exoskeletons if the device has low noise, has simple consistent dynamics from step to step, and does not have a substantial delay between human action and device response.

A potential corollary to the prediction that lowering device noise improves learning reliability is that increasing baseline human exploratory variability compared to unresolved sensorimotor or device noise may improve learning reliability. It is an open question whether baseline exploration as used by the nervous system in implicit learning can be manipulated by an experimenter via purely external means (that is, via sensory or mechanical perturbations or other biofeedback) – in a manner that results in more reliable learning. One study that increased variability externally did not find better learning<sup>64</sup>, while another study increased learning<sup>20</sup>: our model was able to recapitulate the increased learning in the latter study. Another study performed a manipulation that increased both variability and learning<sup>37</sup>. It is unclear if this increased variability specifically corresponds to increased exploration because both studies changed the sensory or the mechanical environment, which could have increased variability by increasing unresolved sensorimotor noise. Further, according to our model, such increased variability comes with a higher energetic cost at steady state<sup>2</sup> as well as potentially higher fall risk, so future work could use our model in concert with targeted experiments to delineate how humans trade-off these competing objectives of exploration, energy, and stability.

Our model naturally predicts the various qualitative features of short-timescale and long timescale responses to perturbations without fitting to the adaptation phenomena being explained. This is in contrast to the single rate or dual rate or memory of errors models of adaptation<sup>9,18,46</sup>, which when applied to locomotor adaptation without including bipedal dynamics and control, do require fits or specific assumptions to capture the direction of both the slow and the fast timescale transients. Here, we predict the short timescale response to sudden perturbations as simply the response of the default stabilizing controller to those perturbations, and this prediction obtains the correct direction or sign of the response without fits to the data it tries to predict. For instance, our model naturally predicts that the immediate transient upon a split-belt perturbation or a leg mass addition is negative step length asymmetry (Figs. 2-4). Similarly, we have shown that a substantial part of slow timescale motor adaptation can be predicted by performance optimization, with energy consumption as the performance objective. This model obtains the correct direction of the slow adaptation without any fits to the adaptation data. In contrast, in the traditional dual rate or memory of errors adaptation models<sup>9,11,18</sup>, the direction of slow adaptation is toward zeroing the error and, therefore, is dictated by how error is defined. Thus, while descriptive models<sup>9,11,18</sup> may be fit to short and long timescale transients in some locomotor adaptation experiments, they do not make predictions of the transients from more primitive assumptions. In addition, we have shown that some common ways of defining error, when coupled with locomotor dynamics, may result in predictions that disagree with experiments.

Our accounting of savings and memory is complementary to previous work that have addressed savings or other related phenomena via memory mechanisms centering on context inference for errorbased learning or for performance improvement<sup>2,41,46,65</sup>. These previous works did not consider the interaction of performance improvement and stabilizing control in a complex task such as locomotion<sup>41,46,65</sup>, as here, or when considering locomotion, did not consider locomotor dynamics and control<sup>2</sup>. Our memory model is also different from models that adapt the 'error sensitivity' (learning rate) of adaptation via a memory of sensory errors<sup>9</sup>, which can capture savings in the form of faster adaptation rates, but is similar to other linear time-invariant state-space models<sup>46</sup> in that neither model can capture savings in adaptation rate after a complete washout<sup>66</sup>.

We have argued that predicting human locomotor adaptation phenomena may require the following functional components: a stabilizing controller, an optimizing reinforcement learner, a gradient estimator, a memory mechanism, and possibly a module that reduces sensory errors. Like all mathematical models of complex phenomena (famously in string theory<sup>67</sup>), there may be multiple realizability: the same architectural hypothesis can be expressed in different terms, grouping some components together, dividing components into their sub-components, or have different realizations of similar function. No matter this multiple realizability, we have shown that a necessary feature of locomotor adaptation is exploration in the neighborhood of a stabilizing controller. Further, the framework implies the existence of a hierarchical separation of timescales of the model components<sup>68</sup>. Specifically, the step-to-step stabilizing controller has the fastest timescale, matching the timescale of the bipedal dynamics to prevent falling: the timescale of gradient estimation must be slower than the step-to-step dynamics so that the estimated gradient is reliable: finally. the timescale of the local reinforcement learner must be slower than the gradient estimator, so that the learner does not change the parameters too quickly for the gradient estimate to be reliable. Human motor learning proceeds over multiple timescales<sup>1,46</sup>, and our approach thus provides a natural functional account of the hierarchy of these timescales from the necessity of stable learning<sup>68</sup>.

Our model of locomotor adaptation is hierarchical and modular. Evidence for the hypothesis of hierarchical and modular motor control goes back to hundred-year-old experiments in which decerebrate cats produced coordinated repetitive movements but not goal-directed movements<sup>69</sup>. It is thought that fast timescale motor responses may be mediated in part by spinal circuits while longer-timescale control, adaptation, and context-dependent responses may be achieved by the interaction of the cerebellum and motor-related areas of the cerebrum<sup>3,24,70,71</sup>. In our model, we have separated the fast timescale stabilizing controller and the slow timescale adaptation mechanisms into distinct interacting modules, so that damage to just the slow timescale adaptation module in the model could still preserve the fast timescale stabilizing response. Such preservation of fast timescale response to treadmill speed changes with degraded slow adaptation to a split-belt condition was found in participants with cerebellar damage<sup>72,73</sup>. Indeed, such studies have established that one locus of such slow timescale motor adaptation, especially involving sensory recalibrations and internal model change, is the cerebellum<sup>3,11,12,72-75</sup>. Thus, while our model is meant to be at the Marr level 1 and 2 (computational and algorithmic levels)<sup>76</sup>, it could inform interpretation of data on neural underpinnings. Conversely, neural data may allow us to fine-tune our model architecture: for instance, modules in the model may contain sub-modules responsible for distinct aspects of behavior

that may be neurally dissociable (e.g., spatial and temporal slow adaptation<sup>44,75</sup>). Some studies have suggested the preservation of 'reinforcement learning' despite cerebellar ataxia<sup>11,13,77</sup>, but such studies examined learning from explicit visual or auditory feedback, which is distinct from the implicit reinforcement learning we have proposed for energy optimization.

Human motor control strategies in highly practiced and learned tasks tend to approximate optimal controllers<sup>78</sup>, and here we have provided an account for how humans gradually learn such optimal controllers in a novel environment. A related learning paradigm is that the nervous system gradually learns an inverse model of the task dynamics from unsuccessful trials, and then uses the inverse model to achieve the task<sup>79</sup>. However, such inversion does not have a unique solution in high-dimensional tasks such as locomotion: human bodies have infinitely many ways to solve a movement task<sup>26</sup> and thus must usually optimize another performance objective to obtain a unique solution. Here, the gradient descent of the stabilizing controller implicitly accomplishes both the inversion and the optimization, as the resulting controller performs the task while optimizing performance.

Our model demonstrates that a local exploration-based search strategy and a simple linear controller structure are sufficient to describe the continuous adaptation of locomotion by human adults to changes to their body and their environment, starting from a known default stabilizing controller, learned under normal conditions. Our approach may lend itself to comparison with the recently popularized framework of deep reinforcement learning<sup>80-82</sup>, which use more expressive controller approximations (deep neural networks) with orders of magnitude more parameters. These methods do not assume initialization with a default controller but instead employ a highly exploratory search involving thousands of discrete walking episodes, often involving falling and resetting the initial condition at the end of each episode. Thus, these learning methods operate in a different regime from our model and are not aimed at explaining gradual human locomotor adaptation.

Most learning requires trial and error, but attempting to improve locomotion via simple trial and error without a stabilizing controller as an inductive bias can result in falling or other learning instabilities. The stabilizing controller in our model allows safe exploration and adaptation, and turning off the stabilizing feedback while the gait is adapted can result in falls or at least substantially degrades learning (Fig. 3). This shows that what control policy the learning acts on determines the effectiveness and safety of the adaptation. We also found that a number of alternative choices can result in falling: prioritizing energy optimization over the near future rather than over a longer time-horizon, too high a learning rate, and updating the gradient estimate too quickly. We have posited the use of exploratory variability for reinforcement learning or optimization, as also suggested in a few studies<sup>2,11,13,38</sup>, including experimental evidence for the role of exploration in improving error-based learning<sup>38</sup>. It was not known how such exploration could be implemented to adapt while walking continuously, without ignoring the locomotor dynamics, stability, and the continuous nature of locomotion (i.e., not treating each step as an independent episode). Indeed, using simple trial and error to perform optimization, for instance, using an exploration-driven search depending on just the previous step<sup>2,13</sup>, works for episodic arm reaching but can result in falling or non-learning for walking with continuous locomotor dynamics. Thus, here, we have put forth a framework for predicting how humans adapt their walking to different conditions while continuing to be stable.

We have tested our model against a wide variety of adaptation studies, providing broad empirical support for the model's predictive ability. Future work can involve the design of targeted experiments to test the different components of this model (e.g., performance objective, adaptation algorithm)<sup>83</sup>, as these components contain heretofore untested assumptions about locomotor adaptation. Here, we have compared the predictive ability of performance objectives such as energy, symmetry, and sensory prediction error, determining what each can predict when acting alone. Future experiments can systematically manipulate the energy landscape, sensory feedback (e.g., vision), and unforeseen perturbations during adaptation to delineate how these performance objectives are traded off by the human nervous system<sup>84</sup> – our model, which allows these adaptation mechanisms to act simultaneously, can provide a framework for interpreting such experiments. Here, we have shown the sufficiency of exploration-based gradient estimation and gradient descent with a fixed learning rate in predicting diverse adaptation phenomena. Future experiments can compare the predictions of gradient descent versus alternative descent or adaptation algorithms (e.g., gradient descent with momentum<sup>39</sup> or learning rate adaptation<sup>9</sup>) in long timescale trials that either have gradually time-varying conditions or alternate between different conditions at various switching frequencies. Such prospective experiments would allow us to characterize the relation between the adaptation direction in experiment and the model-predicted gradient directions, thus helping to modify the model to capture a broader range of experiments. Future work can also test the generality of our framework to other motor adaptation tasks<sup>41,78,85</sup>, including the model's ability to explain savings, generalization, interference, non-learning, and other important phenomena; this application of our model to other motor tasks will require appropriate modifications to the dynamical model and the default controller.

Our focus has been on capturing qualitative phenomena and we did not obtain a quantitative fit by minimizing the error between model predictions and experiment. Indeed, model simplicity may be a sound reason to not seek quantitative fits. While we have captured a wide variety of experimental phenomena from diverse labs, future work could use a higher dimensional musculoskeletal<sup>57</sup> and sensorimotor model and test it against other prior experimental data not considered here<sup>61,86–88</sup> in addition to the aforementioned prospective experiments. In these future studies, we would seek to explain to additional aspects of the experimentally observed adaptation behavior (e.g., detailed kinematics, kinetics, energetics).

Model-based predictions of locomotor adaptation, such as enabled here, have potential applications to improving humanmachine interactions including robotic prostheses and exoskeletons, making such devices intrinsically more learnable or devising protocols for accelerating their learning<sup>57,87,89</sup>. Comparisons of learning in healthy and impaired human populations<sup>54</sup> using our modeling framework provides a means of identifying how distinct hypothesized modules of locomotor adaptation may be affected, potentially informing targeted rehabilitation.

#### Methods

In this Methods section, we first describe the mathematical structure of each component of our modular and hierarchical locomotor adaptation model (Fig. 1), how the components interact, and how this framework is applied to each task setting; the human experiments are described at the end. Human participant research reported herein was approved by the Ohio State University Institutional Review Board and all participants provided informed consent.

#### Stabilizing feedback controller

The mathematical biped model, approximating the human walker, is controlled on a step-to-step basis by a stabilizing feedback controller. The biped model and the stabilizing feedback controller<sup>16,17,26,31,90</sup> are described in greater detail later in this *Methods* section (see also Supplementary Methods). Here, we describe the general structure of the controller necessary to understand our modeling framework. The controller is a function that relates the control variables u (e.g., forces and torques) to the state variables s (positions and velocities). Here, the state s is a vector with as many elements as there are state variables

( $n_{\text{state}}$  elements) and analogously u is a vector with  $n_{\text{control}}$  elements. The control variables have nominal values  $u_{\text{nominal}}$ , sometimes referred to as a 'feedforward' term, which the biped uses in the absence of any perturbations at steady state. Analogously, the state variables also have nominal values  $s_{\text{nominal}}$  in the absence of any external perturbations. Then, on step j, the control variables  $u_j$  are assumed to be related to the state  $s_j$  by the linear equation:

$$u_j = u_{\text{nominal}} + K \cdot (s_j - s_{\text{nominal}}), \tag{1}$$

where *K* is an  $n_{\text{control}} \times n_{\text{state}}$  matrix of feedback gains. This equation (1) is equivalent to the simpler linear expression  $u_j = a + K \cdot s_j$ , which has fewer parameters because the two vector variables  $u_{\text{nominal}}$  and  $s_{\text{nominal}}$  in equation (1) are replaced by the one vector variable  $a = u_{\text{nominal}} - K \cdot s_{\text{nominal}}$ . This vector *a* may be considered the full 'feedforward component' of the controller, in that it contains all terms that do not directly depend on current state. We use the version including  $u_{\text{nominal}}$  and  $s_{\text{nominal}}$  in equation (1), in order to demonstrate the learner's ability to automatically ignore redundant parameters. The linearity of equation (1) is a simplifying assumption, justified by the ability of linear controllers to explain human step to step locomotor control<sup>16,17,25,31,90</sup> and its sufficiency for the adaptation phenomena explained by the framework here. The framework itself does not rely on this assumption of linearity.

#### Local reinforcement learning for performance improvement

When faced with a novel situation, the reinforcement learner changes the parameters of the stabilizing controller to make progress toward a defined objective, expressed as minimizing a scalar objective function or performance objective J evaluated over each stride. The learnable parameters p characterizing the stabilizing controller include unominal, *K*, and *s*<sub>nominal</sub>, i.e. the nominal control and state values as well as the feedback gains. In this study, we only allow the nominal values  $p = [u_{nominal}; s_{nominal}]$  to change during learning. This is because there is a one-to-one mapping between these nominal or feedforward terms and the overall gait kinematic changes we are trying to predict, so allowing the nominal values to change gives the model sufficient flexibility to produce different kinematics. We keep the feedback gains *K* fixed, as the primary role of the feedback term is to keep the system stable despite fast timescale perturbations away from the current gait pattern. Given the robustness of the controller to substantial perturbations<sup>16,17</sup>, this stabilizing role is satisfied by fixed feedback gains K. Indeed, as assumed, we find that changing them is not necessary for the major phenomena discussed herein; allowing just the feedforward term to change<sup>3</sup> is sufficient (e.g., Fig. 2a-d). Allowing the feedback gains K to change may be necessary for even more stabilitychallenging perturbations, where the robustness of the default controller no longer is sufficient – such changes to K can be accomplished with the same framework but would require incorporating the locomotor task constraints explicitly into the performance objective (e.g., not drifting off a finite treadmill, not falling, traveling a certain distance), as otherwise the feedback gains may be chosen in a manner that makes the walker unstable. During learning, we allow the unominal and s<sub>nominal</sub> to change independently for the left and right steps, enabling adaptation to asymmetric conditions.

Fixing the overall structure of the controller during learning to that in equation (1) makes this initial controller structure an inductive bias for learning; that is, it constrains exploration-based learning both by providing an initial condition and restricting the space of controllers explored.

On each stride *i* (every two steps), we denote  $p_i$  to be the current best estimate of the controller parameters. We posit that before encountering a novel condition, the body uses the previously learned controller for normal walking, which we have characterized using data

$$p_{i+1} = p_i - \alpha_g(g_i), \tag{2}$$

where  $g_i$  is the current gradient estimate on the  $i^{\text{th}}$  stride (see equation (7) for how it is estimated) and  $\alpha_g$  is a scalar learning rate for the gradient descent. Rather than executing the next stride using this new  $p_{i+1}$ , we posit that the nervous system uses a perturbed version  $\hat{p}_{i+1}$ :

$$\hat{p}_{i+1} = p_{i+1} + \nu_{i+1} \tag{3}$$

where  $v_{i+1}$  is an exploratory motor noise term, assumed to be multivariate Gaussian noise with standard deviation  $\sigma$ , uncorrelated across time. We posit that the exploratory noise v is intentionally generated by the nervous system, allowing it to estimate the local gradient of the performance objective / with respect to the parameters p, and more generally, build a local internal model of the system<sup>91,92</sup>. This exploration-based estimation of the gradient is in contrast with other simulation-based ways of estimating the gradient, for instance, algorithmic automatic differentiation, also called or backpropagation<sup>24,80</sup>. In addition to this exploratory motor noise, there may be additional unavoidable sensory and motor noise that the nervous system cannot resolve, which we consider later separately<sup>93,94</sup>. The proposed reinforcement learning procedure directly updates the parameters of the control policy via gradient descent, so it may be considered a variant of policy gradient reinforcement learning, where the gradient is estimated as below entirely from exploratory steps<sup>95</sup>. Because the gradient is updated from limited and noisy data (see below), it is a stochastic gradient descent on the control policy. We term this learning 'local' because of its reliance on the information obtained via local exploration in the neighborhood of the controller to make gradual progress toward the optimum. In this formulation, the learnable parameters p are changed every stride, so that the effect of the left and the right step control on the performance objective can be experienced separately before being incorporated into the parameter change. This assumption of once-a-stride parameter change is not essential; the learning framework can be used with continuous phasedependent control<sup>25,31</sup> with more frequent or continuous updates of control parameters.

#### Asymptotic gradient estimate

Estimating the gradient of the performance objective *J* with respect to the parameters *p* is equivalent to building a local linear model relating changes in parameters *p* to changes in performance *J*. This can be understood by noting that a local linear model is the same as a first-order Taylor series, and the gradient  $\nabla_x f$  of a function f(x) about  $x_0$  appears as the coefficient of the variable *x* in this first-order Taylor series as follows:

$$f(x) = f(x_0) + \nabla_x f \cdot (x - x_0) + \text{ higher order terms} \approx \text{ some constant} + \nabla_x f \cdot x.$$
(4)

The performance *J* on a given stride will not only depend on the controller parameters *p*, but the entire system trajectory, which is uniquely determined by the initial system state and the subsequent control actions given by *p*. So, we posit a linear model that includes dependence on both  $s_i$  and  $p_i$ . On stride *i*, if the initial state is  $s_i$ , the parameters are  $p_i$ , and the performance over that stride is  $J_i$ , a linear model

$$J_i = Fs_i + Gp_i + H. \tag{5}$$

Here, coefficient matrix *G* is the gradient of the performance  $J_i$  on the current stride with respect to the learning parameters  $p_i$  and the coefficient matrix *F* is the gradient with respect to initial state  $s_i$ . Building a linear model of  $J_i$  with respect to only  $p_i$ , ignoring the dependence on state  $s_i$  can lead to incorrect gradient estimates and unstable learning.

Performing gradient descent using the matrix *G* as the gradient is equivalent to reducing the performance of a single stride  $J_i$ , without considering the long-term implications. Minimizing just the single-stride performance  $J_i$  may result in unrealistic optima for some performance objectives: turning off the actuators and falling may be optimal when only minimizing energy over one step. So, for non-transient tasks such as steady walking, we hypothesize that the human prioritizes the long-term or steady state performance  $J_{\infty} = \lim_{i\to\infty} J_i$ . This asymptotic or long-horizon performance averages over the noise on any one stride.

To estimate the gradient with respect to long-term performance, the nervous system needs to be able to predict the future. Thus, to predict the long-term consequences of the parameters  $p_i$ , we posit that the nervous system maintains an internal forward model of the dynamics, that is, how the initial state  $s_i$  and the parameters  $p_i$  for a stride affects the state at the end of the stride, equal to the initial state for the next stride  $s_{i+1}$ . This internal model of the dynamics is also assumed to be linear for simplicity:

$$s_{i+1} = As_i + Bp_i + C. \tag{6}$$

Given such an internal model of the dynamics, the nervous system can estimate the future consequences of parameter changes to the steady state (by effectively simulating the internal model to steady state) and thus infer the relevant gradient of  $J_{\infty}$ , given by:

$$g = \nabla J_{\infty} = G + F(I - A)^{-1}B, \tag{7}$$

where the first term *G* gives the gradient of the short-term energy cost over one step, while the second term corrects for the fact that the steady state value of *s* will be different from the current initial state  $s_i$ . This internal model framework also allows the nervous system to minimize performance over an intermediate time horizon by computing and using the gradient of the mean energy cost over the next few strides. We found that minimizing expected performance over just one or two strides into the future can result in unstable learning for energy optimization. In conventional reinforcement learning<sup>95</sup>, a discount factor  $0 < \gamma < 1$  is used to modify the function minimized to  $\sum_{i=1}^{\infty} \gamma^{i-1} J_i$ , which prioritizes near-term performance and down-weights performance in the future. We did not use such a discount factor here, but using  $\gamma \approx 1$  is analogous to the asymptotic limit we have chosen, and  $\gamma$ much less than one will give results similar to optimizing over just the next few strides.

We update the matrices *A*, *B*, *C*, *F*, *G*, *H* on each stride by estimating the linear model via ordinary least squares to best fit the state, the action, and the performance  $(s_i, p_i, J_i)$  over a finite number of previous steps. We used a rolling estimate over 30 steps for all the results presented herein. This gradient estimator needs to have the property that relatively prioritizes recent history<sup>91</sup>, as otherwise, the gradient descent cannot adapt to novel locomotor situations in a timely manner. Using a finite history allows rapid adaptation to sudden changes. Also, we use a linear internal model though the full biped dynamics are nonlinear; a linear internal model is sufficient when adaptation is gradual and the model is constantly updated to be a good approximation about the current operating point.

Learning happens as long as the gradient estimate, however computed, gives a reasonable descent direction on average – that is, gives direction in which to change the control policy to lower the performance objective value. Operating on inaccurate gradients can result in learning instabilities (distinct from instability in the movement dynamics), as can large gradient steps. This learning instability can be prevented in two different ways. First, when the linear models in equations (5) and (6) are inaccurate, as estimated by their residual being outside of the 95% confidence interval at steady state, the learning rate is set to zero. A second approach to avoiding learning instability is a trust region approach, wherein the maximum gradientbased step-size is limited to a fraction the exploratory noise. We tested both approaches and they give qualitatively similar results.

#### Forming motor memories and employing them when useful

We posit a modular memory unit to capture the fact that humans form and maintain memories of previously learned tasks<sup>40</sup>, as opposed to having to re-learn the tasks each time. First, we discuss our model of how such stored 'motor memories' are used, and later in this section, we discuss how these motor memories are formed and updated based on experience.

Consider that the human had some past experience in the current task, and used controller parameters  $p_{\text{memory}}$  with associated performance objective values  $J_{\text{memory}}$ . We posit that humans move toward this memory with some learning rate as follows:

$$p_{i+1} = p_i + \alpha_g \left(-g_i\right) + \alpha_m (p_{\text{memory}} - p_i), \tag{8}$$

where  $(p_{\text{memory}} - p_i)$  is the vector direction toward the memory and  $\alpha_m$  is the rate at which memory is approached. We posit that the controller parameters being learned move toward the memory only when  $J_{\text{memory}} < J_{\text{current}}$ , that is, when progressing toward the memory improves the performance. Secondly, to ensure that progress toward memory does not destroy gradient descent even if  $J_{\text{memory}}$  was inaccurately approximated, we posit that the learning rate  $\alpha_m$  is modulated via a truncated cosine tuning so that memory is used only when the direction toward memory does not oppose the direction of the negative gradient (Fig. 1d). In Supplementary Methods, we elaborate mathematically on why this modulation of the rate toward memory is necessary and sufficient to avoid convergence to a sub-optimal memory.

We conceive of a 'motor memory' as a pair of functions  $F_p(\lambda)$  and  $F_{I}(\lambda)$  that output the controller parameters  $p_{\text{memory}} = F_{p}(\lambda)$  and the corresponding performance objective value  $J_{\text{memory}} = F_I(\lambda)$  respectively, given the task parameters  $\lambda$  (Fig. 1d). The task parameters  $\lambda$ could be continuous-valued, for instance, walking speed or assistance level of an exoskeleton, or discrete-valued<sup>41</sup>, for instance, treadmill versus overground walking or presence versus absence of an exoskeleton. As a simple example, the task parameter could be treadmill belt speed  $v_{\text{belt}}$ , and the stored motor memory functions  $F_p(v_{\text{belt}})$  outputs controller parameters for each walking speed and  $F_{I}(v_{belt})$  outputs the corresponding performance objective value. In this case, the nervous system could infer the belt speed  $v_{\text{belt}}$  from the sensory stream<sup>56</sup>, by fusing proprioception (which can help infer the speed of head relative to foot,  $v_{head/foot}$ ) and vision (which can sense the speed of head relative to lab,  $v_{\text{head/lab}}$ ), so that the belt speed is given by:  $v_{\text{belt}} = v_{\text{foot/lab}}$ =  $v_{\text{head/lab}} - v_{\text{head/foot}}$ . For simplicity, we assume that this task parameter inference is independent of any potential perceptual recalibration<sup>22,42</sup>, which is addressed separately in a later section on proprioceptive realignment.

The memory functions  $F_p$  and  $F_J$  are built over time to approximate the best controllers learned during previous experiences of similar tasks. We posit representations of motor memories via function approximation: in this manuscript, for simplicity, the stored controller parameters  $p_{\text{memory}}$  are linear functions of the task parameters unless

otherwise specified, anchored at a nominal tied-belt condition. Such interpolating function approximations for memory are in contrast to discrete memories of experiences without interpolation<sup>2</sup>: these two assumptions have different testable implications for generalization of learning. The memory functions  $F_p$  and  $F_l$  have memory parameters  $\mu$ , which determine the function approximation, for instance, the slope and intercept of a linear functions  $F_P(\lambda, \mu)$ : here, we allow the slopes of the linear function to change to approximate new experiences, while keeping the intercept at a nominal tied belt walking speed fixed. Analogous to our previous hypothesis that the controller parameters are updated via gradient descent, we posit that these memory parameters are also updated via gradient descent, so that the memory function better approximates controller parameters to be stored. That is, we posit that the nervous system performs:  $\mu_{i+1} = \mu_i - \alpha_{mf} \nabla_{\mu} L$ , where L is a measure of how well the memory approximates the current controller  $p_i$  and  $\alpha_{mf}$  is the learning rate for memory formation; we used the root mean squared error over all controller parameters being approximated. This memory update happens when the current controller  $p_i$  is better than what is already stored in the memory i.e., when  $J_{\text{current}} < J_{\text{memory}}$  or when the direction toward the memory is not a descent direction (Fig. 1d). This makes memory formation and memory use mutually exclusive.

## Minimal walking biped: dynamics, control, energy, and performance

Dynamics. We consider a minimal model of bipedal walking (Supplementary Fig. 1a), consisting of a point-mass upper body and simple legs that can change length and apply forces on the upper body<sup>26,55</sup>. The total metabolic energy cost of walking for this biped is defined as a weighted sum of the positive and negative work done by the stance legs on the upper body and the work done to swing the legs forward<sup>55,96</sup>. For this biped, the periodic energy-optimal walk on solid ground is the inverted pendulum walking gait<sup>26,55,97</sup>, in which the body vaults over the foot in a circular arc on each step (Supplementary Fig. 1b), with the transition from one step to the next achieved via push-off by the trailing leg, followed by a heel-strike at the leading leg (Supplementary Fig. 1c). We use this irreducibly minimal lowdimensional biped model<sup>26,55</sup> to illustrate the predictive ability of our modeling framework for simplicity and transparency. Further, we show that the simple model is sufficient for explaining the major documented locomotor adaptation phenomena in the literature. The locomotor adaptation modeling framework herein can be generalized to a more complex multibody multimuscle model of a human. The parameters of this biped model were not fit to any data from the adaptation phenomena we seek to explain (see Supplementary Methods). When showing metabolic energy cost transients for the model, we show two versions (e.g., in Fig. 2a), one that reflects average metabolic rate over each stride and one that would be measured via indirect calorimetry, which is a low-pass filtered version of the stridewise cost98.

**Stabilizing feedback control**. The biped has two control variables for each leg, namely, step length and push-off magnitude (Supplementary Fig. 1d), for a total of four discrete control actions per stride. These control variables are modulated to keep the biped stable, despite external or internal noisy perturbations and despite a change in the mechanical environment e.g., walking on a split-belt treadmill or with an exoskeleton. The controller keeps the biped stable despite large changes in the body and environment, including external perturbations; this ability to be unaffected by unforeseen changes before any changes to the controller parameters is called robustness, so that the controller is termed 'robust'<sup>16,17,99</sup>. The values of these control variables on each step are decided by a discrete controller, as described below, derived from our prior human experiments on steady walking<sup>16,17,31</sup> without specifically fitting any parameters to the data from the

adaptation experiments we seek to explain. The body state  $s_i$  at midstance at step *i* includes the forward position in the lab frame, the forward velocity in the belt and the lab frame, and the running sum (i.e., discrete integral) of the forward position in the lab frame. The control variables *u<sub>i</sub>* at step *i* are changed by the following linear control rule as a function of the preceding midstance state si  $u_i = u_{\text{nominal}} + K \cdot (s_i - s_{\text{nominal}})$ , where *K* is a matrix of feedback gains<sup>16,31</sup>. The velocity dependence of the control gains ensures that the walker doesn't fall, the position dependence promotes station-keeping<sup>17,31</sup>, and integral dependence reduces error due to systematic changes in the environment, for instance, changing the treadmill belt speeds or going from a tied to a split treadmill. These terms make the controller a discrete PID controller (proportional-integral-derivative). The nominal periodic motion at each speed is governed by the feedforward pushoff and step length values, and these are selected so as to have the same speeds and step lengths as a typical human (Supplementary Fig. 2). The default values for the control gain matrix K are then obtained by fitting the dynamics of the model biped to the step to step map of normal human walking on a treadmill<sup>16,17,31,90</sup>. Mathematical details and parameter values are provided in the Supplementary Methods. All variables in equations and figures are non-dimensional, unless otherwise mentioned: lengths normalized by leg length  $\ell$ , masses normalized by total body mass, and time normalized by  $\sqrt{\ell/g}$ , where g is acceleration due to gravity<sup>55</sup>.

Different locomotor task settings. The biped model described above is expressive enough to capture the different task settings for which we seek to model adaptation: walking with different exoskeleton assistance protocols, at varying belt speeds (tied or split-belt), and with asymmetric leg masses. Here, we briefly describe how the different conditions are simulated by changing the external environment and force it exerts on the biped. See Supplementary Methods for mathematical details. The model described above allows the individual treadmill belt speeds to be changed as a function of time (Fig. 2a,c). This generality is sufficient to simulate both split-belt and tied-belt treadmill walking conditions. The total metabolic cost computed accounts for individual belt-speed changes because all components of the metabolic cost, namely, push-off work, the heel-strike work, and the leg swing cost are computed by incorporating the relevant beltspeeds and effective leg masses. For split-belt walking protocols, we usually use non-dimensional belt speeds of 0.5 for the fast belt and 0.25 or 0.3 for the slow belt for many but not all computational results (Figs. 2a, 4-8): these walking speeds and their durations may be different from precise experimental conditions but the qualitative features we illustrate are insensitive to such differences in speeds chosen. We simulated exoskeletons as external devices in parallel to the leg that produces forward forces, or equivalently, ankle torques (Figs. 2d and 4e). Walking with periodic exoskeleton input used the perturbation as an additional input state in the controller. For predicting adaptation to foot mass change (Fig. 2b), we incorporated the simplest leg swing dynamics: a point-mass foot, propelled forward with an initial impulse and the foot mass coasting forward passively until heelstrike. For the tied-belt walking, we used the belt speed as the task parameter; for split-belt studies, we used the individual belt speeds as the task parameters; for the added leg mass study, we used the added leg mass as the task parameter. To track gait asymmetry, we use the following two objectives of left-right asymmetry<sup>4</sup>, namely step length asymmetry and step time asymmetry, defined as follows:

step length asymmetry = 
$$\frac{D_{\text{fast}} - D_{\text{slow}}}{D_{\text{fast}} + D_{\text{slow}}}$$
 and step time asymmetry =  $\frac{T_{\text{fast}} - T_{\text{slow}}}{T_{\text{fast}} + T_{\text{slow}}}$ ,  
(9)

where the fast and the slow step lengths ( $D_{\text{fast}}$  and  $D_{\text{slow}}$ ) are defined at heel strike as in Supplementary Fig. 1e and the step times  $T_{\text{fast}}$  and  $T_{\text{slow}}$ 

are the stance times when on the fast and slow belts respectively. We use analogous measure of asymmetry when the biped walks with an asymmetric foot mass, but different from that used in the experimental study on foot mass adaptation<sup>5</sup>. There can be other ways of quantifying asymmetry and we chose asymmetry objectives that are commonly used to empirically track adaptation<sup>4,5,45</sup>. A zero value indicates symmetry with respect to these measures, but does not imply perfect left-right symmetry of the entire motion.

All computational work was performed in MATLAB (version 2022a). See Supplementary Methods and our codebase implementing these simulations, *LocAd*<sup>30</sup>, shared via a public repository. Digitized data from prior manuscripts<sup>5,6,8,18,20,28,36,45,48,52,100</sup> are plotted in Figs. 2 and 7b and Supplementary Figs. 2, 5, 6, as cited in place, simply to illustrate whether model-based predictions agree qualitatively with experimental results in prior studies.

#### Alternative to performance optimization: Comparison with proprioceptive realignment

Experimental evidence during split-belt adaptation suggests some recalibration of proprioception by the two legs<sup>42</sup> and has been argued to be at least partially responsible for kinematic adaptation<sup>22,42</sup> based on the correlation of timescales between such realignment and adaptation. No mathematical model been previously proposed for how such realignment may happen. Without such a mathematical model, it is impossible to know whether the direction of adaptation due to such realignment will be consistent with or opposing that observed in the experiment. Here, we first present such a mathematical model and then test the extent to which it explains adaptation on a split-belt treadmill. We implement this proprioceptive realignment as a gradual sensory recalibration of the input to the stabilizing controller, replacing the gradient-based reinforcement learner (Fig. 9a–b).

Recalibration takes place when there is substantial conflict between what is expected by the nervous system and what is sensed<sup>11</sup>. The key missing hypothesis in extending such sensory recalibration to locomotor adaptation lies in the question: what error is the nervous system using to drive recalibration during locomotion? We hypothesize that, given the typical walking experience in daily life, the nervous system expects the two legs to be on a common surface: this expectation results in a sensory conflict on a split-belt treadmill with both feet experiencing unequal belt speeds.

When the walking surface has fixed speed and the visual environment is uniform, the walking speed can be estimated by the nervous system by two sensory modalities<sup>56</sup>: vision (based on visual flow) and proprioception (by integrating joint angles and angle rates from muscle spindles and Golgi tendon organs). On a treadmill in a lab, vision has information about how the head moves with respect to the lab, so we identify the visual speed with  $v_{\text{body/lab}}$ . Proprioception has information about how fast the body parts move relative to the stance foot on the belt, so we identify proprioception with  $v_{\text{body/belt}}$ . Thus, the body has information to implicitly estimate the belt speed via the following equation:  $v_{\text{belt/lab}} = v_{\text{body/lab}} - v_{\text{body/belt}}$ . On a split-belt treadmill, all these speeds will be belt-specific, e.g., v<sub>belt,1/lab</sub> and  $v_{\text{belt.2/lab}}$ . The expectation that both legs contact a common surface can be expressed as the equality of these individual belt speeds:  $v_{\text{belt,1/lab}}$ =  $v_{\text{belt,2/lab}}$ . We posit that deviations from this equality result in slow recalibration. Consistent with much of the arm reaching literature, we recalibrate only the proprioceptive sense, hence the term proprioceptive realignment.

Say,  $\bar{\nu}_{\text{body/belt,1}}$  and  $\bar{\nu}_{\text{body/belt,2}}$  are the proprioceptively obtained sensory information from the two legs without recalibration, and  $\hat{\nu}_{\text{body/belt,1}}$  and  $\hat{\nu}_{\text{body/belt,2}}$  are the recalibrated versions. The two versions are related by:

$$\hat{v}_{\text{body/belt, 1}} = \bar{v}_{\text{body/belt, 1}} - \Delta v_1 \text{ and } \hat{v}_{\text{body/belt, 2}} = \bar{v}_{\text{body/belt, 2}} - \Delta v_2, \quad (10)$$

where  $\Delta v_1$  and  $\Delta v_2$  are the recalibrative corrections. We describe this recalibration as happening via a state observer with two timescales: a fast timescale process estimating a common belt speed  $\hat{v}_{common}$  using proprioceptive information from both legs and a slow timescale process estimating the recalibrative corrections  $\Delta v_1$  and  $\Delta v_2$  for each leg separately. The common belt speed estimate is updated every step *j* via a state observer as follows:

$$\hat{v}_{\text{common}}(j+1) = \hat{v}_{\text{common}}(j) + a_{\text{common}}\left(\bar{v}_{\text{body/lab}}(j) - \bar{v}_{\text{body/belt},k}(j) - \hat{v}_{\text{common}}(j)\right)$$
(11)

where k equals 1 or 2 for odd and even step number given by  $i_i$ respectively, and  $a_{\text{common}}$  is a rate constant proportional to the time spent on each step - but we treat as constant for simplicity. This equation results in convergence of  $\hat{v}_{common}$  to the average belt speed. The recalibration  $\Delta v_k$  is the current estimated perturbation of the individual belt speed from the estimated common speed  $\hat{v}_{\text{common}}$ . recalibration is updated This on every stride i as  $\Delta v_k(i+1) = \Delta v_k(i) + a_{\Delta}(\bar{v}_{\text{body/lab}} - \bar{v}_{\text{belt, k/lab}} - \hat{v}_{\text{common}} - \Delta v_k(i)).$ Here. the rate constant  $a_{\Delta}$  is much smaller than  $a_{\text{common}}$ , reflecting the slower timescale at which the perturbation estimate  $\Delta \hat{v}_k$  is updated. Here,  $\hat{v}_1$  is updated on odd steps and  $\hat{v}_2$  is updated on even steps. This perturbation estimate  $\Delta v_k$  eventually converges to the deviation of the actual belt speed from the common speed. These state observer equations for recalibration are similar to estimating the belt speed via a state estimator reflecting an expectation that tied-belt changes are much more likely than split-belt changes, modeled by the noise covariance matrix for belt speed changes having large diagonal elements (governing co-variation of belt speeds) and small off-diagonal elements (governing belt speed differences). Further, while we have introduced the latent variables  $v_{common}$  and  $\Delta v_k$  in the above description, the recalibration equations can be written without such latent variables. The recalibrated proprioceptive information  $(\hat{v}_{\text{body/belt,1}} \text{ and } \hat{v}_{\text{body/belt,2}})$  is used in the stabilizing controller instead of the direct proprioception. In the Results, we show effects of 50% and 100% recalibration: 100% corresponds to using the full correction  $\Delta v_k$ and 50% uses  $0.5 \Delta v_k$  in the recalibration equation (10).

## Alternative to energy minimization: Comparison with reducing kinematic task error

Minimizing kinematic task error first requires defining what the desired or expected kinematics are. To define this, we first note that slow timescale error minimization is not thought to underlie tied-belt walking adaptation, or at least the timescales of adaptation to tied-belt speed changes are much faster than for split-belt adaptation<sup>28</sup>. So, we posit that the nervous system treats tied-belt walking – or walking on the same surface with both legs – as the normal state of affairs, basing the desired kinematics on an implicit assumption of tied-belt walking. The nervous system estimates the common belt speed  $\hat{v}_{common}$  as in the previous section, using visual flow and proprioception from both legs (see eq. (11) and Fig. 8b). This common belt speed  $\hat{v}_{common}$  is then used to make a prediction for the body midstance state  $\hat{s}_{common}$  based on memory, which is compared with actual sensory information  $\bar{s}$  to compute the task error  $E = \hat{s}_{common} - \bar{s}$ .

In simple tasks such as arm reaching, where both the error and the action is one-dimensional, it is possible to reduce error via a simple 'error-based learning model' with a single or dual rate process<sup>46</sup> or via learning rate adaptation<sup>9</sup>. However, in tasks such as walking in a novel environment, because body state and the number of actuators is high-dimensional, the nervous system may not have a priori inverse model to produce the motor actions that reduce the error. So, a simple one-dimensional error-based learning model is not appropriate. We instead model the error reduction as proceeding analogous to energy reduction via gradient descent using exploratory variability to estimate gradients, as a special case of the framework in Fig. 1. The kinematic

task error being minimized may also be considered a kind of sensory prediction error, as the error from the kinematic state predicted or expected by the nervous system given the belt speed estimate.

#### Interaction with explicit control

The mechanisms proposed herein are for implicit adaptation, but these mechanisms allow for explicit (conscious) control acting in parallel to implicit adaptation. We show how our model can be extended to interact with explicit input by implementing an visuallyinformed explicit control module for the reduction of step length asymmetry<sup>10</sup>. On each step, the explicit control module outputs a correction to the desired step length proportional to the step length asymmetry on the previous stride, with the intention of reducing the step length asymmetry on the current step. This output from the explicit control module is added to the desired step length output from the implicit adaptation module (the default adaptation mechanisms here), so that the net total control input is used by the stabilizing controller. The additive and parallel nature of the implicit and explicit modules are as proposed for explicit control in arm reaching studies<sup>23</sup>. The architecture of the proposed interaction between the implicit adaptation and explicit control is such that the implicit module is only aware of its own output and not that of the explicit module; thus, the implicit module optimizes the objective with respect to its own output.

#### **Prospective experiments**

The computational model we put forth here can be used to design prospective experiments, augmenting experimenter intuition. Here, we conducted two model-guided experiments to test predictions of the model that are surprising when compared to the existing literature: (1) on the effect of environment noise on locomotor adaptation, and (2) on the effect of an immediately preceding counter-perturbation on a subsequent adaptation.

Twenty-five participants (19 male, 6 female, self-reported sex, age 21.9  $\pm$  3 years, mean  $\pm$  s.d.) participated with informed consent and the experiments were approved by the Ohio State University IRB. Participants were assigned randomly into two groups: sixteen participants performed experiment 1 (12 male, 4 female, age 21.7  $\pm$  3 years) and nine participants (6 male, 3 female, age 22.3  $\pm$  3 years) performed experiment 2. Both experiments involved walking on a split-belt treadmill (Bertec Inc.), with the details of the protocol provided below. Foot movement was tracked via a Vicon T20 motion capture system (Vicon Nexus 1.x). Sex or age was not used as an explanatory variable in any analysis, as the computational model tested does not include such variables.

Experiment 1 was designed to test the model prediction that when the belt noise level was sufficiently high, learning can be degraded, which is surprising relative to a prior finding that a modest level of belt noise can slightly enhance learning as measured by after-effects<sup>20</sup>. For this experiment, the participants were sub-divided into two groups of eight: one group performed a no-noise abrupt protocol (Fig. 7a), in which participants started walking under tied-belt conditions at 0.9 m/s, then adapted to split-belt condition of 0.6 m/s and 1.2 m/s kept constant for 10 minutes, followed by three minutes of tied-belt walking at 0.6 m/s; the second group had an identical protocol except the split-belt condition involved continuously changing belt speed for just the fast belt, fluctuating in a piecewise linear manner with zero mean and 0.2 m/s standard deviation (normally distributed). The consecutive grid points of the piecewise linear noise were separated by 1.2 seconds, roughly equal to a stride period, so that the noise value was different two strides apart (the noise in<sup>20</sup> was changed every 3 seconds, and thus had greater temporal correlation); speed changes had 0.1-0.2 m/s<sup>2</sup> accelerations. The noise standard deviation was set at a lower level in simulation (0.04 m/s) to ensure stability. The postadaptation after-effect in step length asymmetry after baseline

Experiment 2 was designed to test the model prediction regarding savings, specifically whether experiencing a counter perturbation B beforehand, interferes with adaptation to perturbation A. Previous experiment<sup>52</sup> had found that if B and A were separated by a washout period, the adaptation to A was not significantly affected compared to not having experienced B. Our model had a distinct prediction for when A immediately followed B, without a washout period W. So, participants performed this experimental protocol T-B-A (Fig. 6) in which 4 minutes of walking on a tied-belt at 0.9 m/s (T) was followed by a split-belt condition with belt speeds of 0.6 and 1.2 m/s for 10 minutes (B), immediately followed by the opposite split-belt condition 1.2 and 0.6 m/s for 10 minutes (A). Equivalent to comparing the A of protocols T-A and T-B-A by bilateral symmetry, we compared the initial transient and the time-constant of the two adaptation periods B and A in T-B-A: the B of T-B-A was without prior split-belt experience and the A of T-B-A is the adaptation phase just after a counter-perturbation.

#### **Reporting summary**

Further information on research design is available in the Nature Portfolio Reporting Summary linked to this article.

## Data availability

The experimental data generated in this study have been deposited in the Dryad database<sup>101</sup> with https://doi.org/10.5061/dryad.kh18932gq. Other human experimental data or results referred to herein are available in previously published manuscripts<sup>5,6,8,18,20,28,36,45,48,52,53,100</sup>.

### **Code availability**

Code associated with this paper, *LocAd*<sup>30</sup>, is available at: https://doi.org/10.5281/zenodo.13887633, which links to a public Github repository.

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## Author contributions

N.S. initially conceived the central question. N.S. and M.S. conceived the theoretical framework, created mathematical models, performed computations, analyzed the results, and wrote the manuscript. B.C. contributed additional models and calculations. All authors reviewed and approved the manuscript.

### **Competing interests**

The authors declare no competing interests.

## Additional information

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## Supplementary Information for "Exploration-based learning of a stabilizing controller predicts locomotor adaptation"

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## **Supplementary Figures**



**Supplementary Figure 1. Biped model and controller. a)** A minimal biped model with a point-mass upper body, **b**) using an inverted pendulum walking gait, **c**) with step to step transitions mediated by impulsive push-offs and heel-strikes<sup>1,2</sup>. **d**) The push-off and step lengths on every step are controlled via state feedback on center of mass state, so that moving faster than desired or being behind the desired position results in a larger push-off and a smaller step length<sup>3–5</sup>. **e**) The step length asymmetry is computed based on step lengths  $D_{\text{fast}}$  and  $D_{\text{slow}}$  (distance between the feet) measured at the time of heel-strike onto the fast or slow belt in the case of split-belt walking. For walking with an asymmetric foot mass, an analogous step length asymmetry is computed by using step lengths  $D_{\text{heavy}}$  and  $D_{\text{normal}}$  onto the heavier foot and the normal foot respectively.





**Supplementary Figure 2.** Steady state walking characteristics. At each steady walking speed, humans use a stereotypical step length — or equivalently, step frequency and step time, derivable from speed and step length<sup>6,7</sup>. One parameter of the biped model (scaling of swing cost) is chosen such that the optimal gait captures how the steady step length, step frequency, and step time change with speed in human data<sup>6,7</sup>.



Split-belt walking: Energy landscape is shallower and has less curvature along step length asymmetry than step time asymmetry

**Supplementary Figure 3.** Step length vs step time asymmetries. For walking on a split-belt treadmill, the energy landscape has optimum at positive step length asymmetry and positive step time asymmetry. The curvature and thus the slopes are higher along the step time asymmetry than the step length asymmetry directions, thus predicting that gradient descent-based learning will converge faster in step time asymmetry rather than step length asymmetry. Further, the relative flatness of the optimum along step length asymmetry compared to along step time asymmetry means the behavior can be further from the optimum along step length asymmetry direction for a given energy penalty. So, if the learning does not converge fully, we expect it to be further away from the optimum along the step length asymmetry can be chosen in infinitely many ways, for instance, with different total or average step lengths; so this would need to be a higher dimensional plot to get a better characterization of the energy landscape. We have shown two slices of this higher dimensional cost landscape to compare the curvatures along two directions in the units chosen; the slices are chosen through the optimum, with the other free variables chosen to be their optimal value given the appropriate step length or step time asymmetry value.





**Supplementary Figure 4. State-dependent exoskeleton assistance.** a) Forward assistive torques are applied by the exoskeleton starting at fixed leg angles, with the torque being angle dependent. This makes the assistance periodic in gait phase defined based on leg angle. b) The reinforcement learner learns to take advantage of the assistive pulls by changing the step timing slightly, with the transient being due to both the stabilizing feedback controller and the reinforcement learner. Period when the exoskeleton is providing perturbations is shaded light blue. Perturbations were applied at leg angle equalling -0.1 radians, where an angle of 0 corresponds to a vertical leg. Accelerating and decelerating perturbations both result in periodic gaits, but with periods lower or higher than the nominal gait period.

#### Learning a task generalizes to neighboring tasks



Model predicts qualitative effect of perturbation size on initial transient and eventual steady state c) Bigger perturbation implies bigger initial transient and more positive steady state



**Supplementary Figure 5.** Generalization to neighboring tasks and size dependence of transients. a) Learning a new task generalizes to neighboring tasks. Learning a larger split A and then learning a smaller split B with tied-belt washout W in between (protocol A-W-B) results in a faster learning transient for task B rather than learning B directly (protocol B), as seen in experiments<sup>8</sup>. Light blue shaded regions indicate adaptation regions for whom behaviors are compared. b) Learning a larger split A and then learning a smaller split B, with a tied-belt washout W in between (protocol A-W-B) can result in faster re-learning transient for B than learning B first and then re-learning B with a washout in between (protocol B-W-B), as in experiments<sup>8</sup>. These phenomena are due to the interpolative function approximation properties of the memory and constitute savings from experience with neighboring tasks. c) The model is able to capture, qualitatively, how the initial transient and the eventual steady state change based on the size of the belt-speed splits<sup>8</sup>.



Supplementary Figure 6. Protocols with abrupt, gradual, and extended adaptation regimes. a) We simulated the different adaptation protocols consisting of gradual and abrupt introduction of a split-belt condition, different extents of the adaptation regime, and gradual versus abrupt ending to the adaptation regime, analogous to those considered by Roemmich and Bastian<sup>9</sup>. Different speed change protocols have different color shadings, and the behavior in panels b and c use the same colors. b) During first adaptation, the protocols that begin with abrupt change in belt speeds showed qualitatively different transients compared to the protocols with gradual changes in belt speeds: specifically, the abrupt adaptation phases had an initial negative step length asymmetry that slowly became less negative; the gradual adaptation phases had an initial zero step length asymmetry that slowly became more negative. These qualitative differences in experimental data were predicted by the model for appropriate model parameters. c) The model predicts that the second adaptation of every other protocol will have a smaller initial transient and more savings than 'gradual' protocol, as is qualitatively seen in the experimental data. Further, the longer duration abrupt first adaptation resulted in a smaller initial transient during second adaptation compared to a short abrupt protocol, both in the model and data. In this manuscript, we have commented mainly on qualitative results that are robust to model and protocol parameter choice and have not attempted quantitative fits. However, some other results — such as the relative ordering of savings between 'abrupt' and 'extended gradual' in this figure – are dependent on details of the model or experiment. One can change this ordering either by changing model parameters, or by changing the 'extended' duration of the 'extended gradual' protocol. Such sensitivity to experimental parameters is a falsifiable prediction that can be tested by further experiment.

![](_page_28_Figure_0.jpeg)

Delay between input x and objective f(x) can degrade or stop gradient descent learning

**Supplementary Figure 7.** Delay degrades or stops adaptation. Exploration-based gradient descent to optimize an objective function f(x) with and without delay. Blue shaded region is when the optimization process is turned on. **a**) Without delay between *x* and f(x), the gradient is estimated reliably and gradient descent proceeds to reduce the function value. Twenty different optimizations are shown from the same initial condition, and same levels of exploratory and sensory noise levels. **b**) With a delay of one step between the input *x* and function values f(x), learning via gradient descent is completely stopped in some trials and is severely degraded in other trials. See *Supplementary Methods*. This delay-based degradation of learning is largely independent of the nominal energy gradients.

Figure	Quantities compared	t(df)	p	Cohen's d	Paired	Tailed	Non-	Normality
							parametric	;
							р	
5	Model: time constants of	21.8(9)	< 0.001	9.62 (5.95, 16.18)	yes	yes	0.002	yes
	first and second adaptation							
6a	Model: initial transient in A in TATATA vs TATBTA	0.244(18)	0.810	0.104 (-0.74, 0.94)	no	no	0.678	yes
6a	Model: early change in A in TATATA vs TATBTA	-0.114(15)	0.911	-0.049 (-0.89, 0.79)	no	no	0.910	yes
6b	Model: rate constant of B and A in TBA	-1.42(7)	0.200	0.066 (-0.21, 0.048)	yes	no	0.250	yes
6b	Experiment: rate constant of	-0.363(8)	0.726	-0.11 (-0.70, 0.49)	yes	no	1	yes
	B and A in TBA							
6b	Model: initial transient of B and A in TBA	-37.4(7)	< 0.001	-18.1 (-32.9, -10.6)	yes	no	0.008	yes
6b	Experiment: initial transient of B and A in TBA	-3.36(8)	0.005	-0.98 (-2.10, -0.25)	yes	no	0.006	yes
7a	Model: after-effect noisy and no noise	2.86(11)	0.0154	1.13 (0.28, 1.96)	no	no	0.001	yes
7a	Experiment: after-effect noisy and no noise	-2.41(14)	0.0151	-1.14 (-2.14,-0.11)	no	no	0.0249	yes
7b	Model: gradual no-noise and gradual noisy	3.59(12)	0.0035	1.42 (0.53, 2.28)	no	no	0.0051	yes
7b	Model: gradual no-noise and abrupt no noise	11.9(22)	< 0.001	4.68 (3.09, 6.24)	no	no	< 0.001	yes
7b	Model: gradual noisy and abrupt no noise	0.16(12)	0.875	.063 (-0.71, 0.84)	no	no	0.371	yes

**Supplementary Table 1. Details of statistical comparisons.** Column 1 refers to the figure number in the main manuscript, in which the corresponding data are plotted. Details reported in columns 3, 4, 6, and 7 are for *t*-tests: t(df) indicates the *t* statistic, with the number of degrees of freedom for the *t* test in parenthesis; *p* refers to the *p* value for the *t*-test. Tailed *t*-tests are always in the direction of difference predicted by the model. Normality of samples was tested and we found that the null hypothesis of normality was not rejected at the 5% level for any of the samples. In addition to *t*-tests, *p* value for non-parametric tests that do not rely on normality are provided. In every occurrence, the non-parametric test agreed with the t-test at the 0.05 significance level. See *Supplementary Methods* for more details.

## **Supplementary Methods**

#### Biped model, feedback controller, learning, and parameters

We now provide further mathematical details for the biped model<sup>10</sup>, controllers, and learning.

**Equations of motion.** When the foot is fixed in an inertial frame, the inverted pendulum phase of inverted pendulum walking (Supplementary Figure 1a-b) has the following equations of motion:

$$m\ell^2\ddot{\theta} + mg\ell\sin\theta = \tau,\tag{1}$$

where  $\theta$  is the stance leg angle from the vertical, *g* is the acceleration due to gravity,  $\ell$  is the leg length, *m* is the point mass body, and  $\tau$  is an ankle torque; clockwise and rightward are positive. These equations apply whether the inverted pendulum walking happens overground or on a treadmill, as long as the treadmill belt holds constant speed. A purely forward force *F* on the center of mass, such as from an external device or the inertial forces from belt acceleration, is achieved by having  $\tau = F\ell \cos \theta$ . Thus, when the belt is accelerating forward with acceleration  $a_{belt}$ , the equation of motion is:

$$m\ell^2\ddot{\theta} + mg\ell\sin\theta = -ma_{\text{belt}}\ell\cos\theta.$$

•

(2)

**Push-off and heel-strike.** During the step to step transition (Supplementary Figure 1b-c), push-off happens first. The leg direction  $\hat{n}$  is initially perpendicular to the body velocity  $\bar{v}$  with respect to the current stance belt just before push-off. During push-off, if the push-off impulse is positive, the velocity is such that  $\hat{n} \cdot \bar{v} \ge 0$ , so that push-off only does positive work. If the push-off impulse magnitude is  $I_{\text{push-off}}$ , the post-push-off velocity in the push-off belt frame is  $\bar{v} + \Delta \bar{v} = \bar{v} + I_{\text{push-off}} \hat{n}/m$ . The positive work performed by the leg is equal to the kinetic energy change in the push-off belt frame, which is also equal to  $m(\Delta v)^2/2$ , because of pythagorean theorem<sup>11</sup>. This quantity is equal to the work performed by a telescoping leg.

The analysis of heel-strike is the reverse of push-off. After heel-strike, the body velocity is again perpendicular to the new stance leg, now on the heel-strike belt. If the body velocity just before heel-strike in the heel-strike belt frame is  $\bar{v}$  and the heel-strike leg direction is now  $\hat{n}$ , the post-heel-strike velocity in the heel-strike belt frame is  $\bar{v} + \Delta \bar{v} = \bar{v} - (\bar{v} \cdot \hat{n})\hat{n}$ . Here, the second term  $(\bar{v} \cdot \hat{n})\hat{n}$  is the component of pre-heel-strike velocity along the heel-strike leg, which is entirely lost upon heel-strike. The leg only performs negative work during such a heel-strike. The value of this negative work equals the change in kinetic energy across the heel-strike, computed in the frame of the belt onto which heel-strike happens, given by:  $-m(\bar{v} \cdot \hat{n})^2/2$ .

**Metabolic energy cost.** The metabolic energy cost  $E_{\text{step}}$  for each step is a sum of two terms, a stance leg cost  $E_{\text{stance}}$  and a leg swing cost  $E_{\text{swing}}$ . That is,

$$E_{\text{step}} = E_{\text{stance}} + E_{\text{swing}}.$$
(3)

The stance leg cost captures the metabolic cost of the mechanical effort during stance, and we set it equal to

$$E_{\text{stance}} = b_{\text{pos}} W_{\text{pos}} + b_{\text{neg}} |W_{\text{neg}}|, \tag{4}$$

where  $W_{\text{pos}}$  and  $W_{\text{neg}}$  are, respectively, the push-off positive work and the heel-strike negative work, and  $b_{\text{pos}} = 4$  and  $b_{\text{neg}} = 0.83$  are reciprocals of the positive and negative work efficiencies<sup>1,12,13</sup>. For the leg swing cost, we initially considered two versions of the model: (1) a work-based swing cost, based on the mechanical work needed to move a point foot by a given distance in a given amount of time, starting and ending at the respective belt speeds; this cost used the same weighting of positive and negative work as for the stance  $\cot^{10,11,13,14}$ ; (2) an empirical swing cost due to Doke and Kuo<sup>15</sup> where the cost scales with the typical force rates required for the point-mass to traverse a given distance in a given time<sup>11,13,15</sup>. We confirmed that the qualitative step length asymmetry adaptation behavior for the split-belt adaptation was similar for the two swing costs, and then for the rest of the manuscript, used the latter force-rate-related cost given by the following equation:

$$E_{\text{swing}} = c_{\text{swing}} \left| \frac{\Delta v}{\Delta t} \right| \cdot \frac{1}{\Delta t},\tag{5}$$

where  $\Delta t$  is with the swing duration and  $\Delta v$  is the change in the foot speed from stance (when the foot moves with the belt) to swing (when the foot moves with speed needed to cover the distance between the foot placements within the swing duration). The multiplier for the swing cost  $c_{swing} = 0.9$  was chosen to approximate the speed-step-length relationship in normal walking (Supplementary Figure 2).

The metabolic rate over a stride (two steps) is the metabolic cost divided by the stride time. For purely visualization purposes, from this stride-wise metabolic rate  $\dot{E}_{stride}$ , we predict what would be measured via indirect calorimetry  $\dot{E}_{VO2}$ , obtained by filtering the stride-wise metabolic rate with a first order linear process with a time-constant of 42 seconds (as in<sup>16,17</sup>). That is,

$$\dot{E}_{\rm VO2} = \lambda \cdot (\dot{E}_{\rm stride} - \dot{E}_{\rm VO2}) \tag{6}$$

where  $\lambda$  is the reciprocal of the time constant. Such predicted metabolic equivalents of indirect calorimetry is denoted as measured by VO2 in Fig. 2 in the main manuscript.

**Feedback controller.** The inverted pendulum walker has only two control variables for each step (Supplementary Figure 1d): the push-off impulse *I* and the step length *d*, so that the control variable u = [I;d]. These two control variables are modulated based on deviations in body state to keep the biped stable. The feedback controller is of the form:  $u = u_{nominal} + K(s - s_{nominal})$  or equivalently u = a + Ks, with  $a = u_{nominal} - Ks_{nominal}$ , where *s* is the relevant body state and *K* is a matrix of feedback gains. The state *s* is composed of four variables: the body velocity in the belt frame, body velocity in the lab frame, the body position in the lab frame, and the sum of past body positions in lab frame, all at midstance, that is when the body is over the foot ( $\theta = 0$ ). This controller has the structure of a discrete *PID* control, with feedback on position (proportional term), velocity (derivative term), and sum of positions (integral term). The feedback on the body position and the sum of past body positions help with station-keeping on the treadmill, that is, not drift off the treadmill. We use the discrete sum instead of

the integral because the control is discrete and once-per step, rather than continuous. The parameters  $u_{nominal}$ , K, and  $s_{nominal}$  for the default controller are obtained from steady walking data, so as to approximate the step to step maps, as in<sup>3–5</sup>. This fit has one additional input from those in<sup>3,4</sup> and uses slightly different relative weighting for matching the step to step map – but the differences are unimportant for the qualitative results herein. The specific gain parameters are in Supplementary Table 2.

By default, we use the state at mid-stance to select the next push-off and step length, because in most simulations here, there is no additional perturbation between midstance and heelstrike<sup>3–5</sup>. Just for the case where there are impulsive exoskeletal input, instead of basing the control on the mid-stance state, we allow the target push-off and step length on the next step to be continuously updated through the stance phase until the leg angle corresponds to the proposed step length. This continuous updating of the proposed control is performed so as to account for any additional perturbations between mid-stance and heel-strike. We perform this continuous updating so as to exactly conserve the overall step-to-step dynamics of the mid-stance based control: specifically, we continuously update the control based on the current angular velocity by computing the corresponding previous mid-stance angular velocity and then using the mid-stance-based controller to decide the next push-off and step length.

**Leg swing dynamics.** In the aforementioned model description, the swing legs had no explicit dynamics coupled to the rest of the body, but were directly controlled by the feedback controller by specifying the next foot placement. This is a simple modeling choice with a rich tradition of explaining a variety of locomotor phenomena<sup>11, 14, 18</sup>. Despite the lack of explicit leg-swing dynamics, the model has a leg swing cost that is computed from the distance and duration between foot placements, as mentioned in the previous paragraph on metabolic cost.

Simulating the addition of asymmetric foot mass requires explicit leg swing dynamics and control, so the dynamics have an additional degree of freedom in this case. For this situation, we use a minimal dynamical model of leg swing in which the leg swing is initiated by a hip impulse and then coasts passively until heel-strike, as suggested by classic leg swing EMG data<sup>18,19</sup>. This impulse is an additional control variable and the initial leg swing state is an additional state variable. The controller is chosen, as earlier, such that the model has the closest return map to the empirical human step to step dynamics at steady state. In this case, the detailed feedback gain parameters are different from that in Table 2 but the overall controlled locomotor dynamics are approximately the same by construction, so the controller is considered effectively the same. Because the belt speed is fixed here, it is not essential to use controller gains for speed relative to the belt frame and the lab frame. Here, the swing leg dynamics are coupled to the center of mass only through the foot placement<sup>20</sup> and thus the nominal gait for this biped with leg swing is identical to the pure inverted pendulum walking gait considered earlier without leg swing dynamics.

**Walking with exoskeleton torques.** All exoskeleton simulations used the inverted pendulum walking model as described above. For all the exoskeleton calculations considered here, the treadmill belt speed is fixed, so separated controller gains for speed relative to the belt frame and the lab frame Table 2 was not needed, but just the sum of their gains assigned to the speed relative to the belt is sufficient.

We conceived the exoskeleton as providing a torque about the foot, which — for this simple model — can help simulate forward pulls, slopes, ankle torques, and hip torques. We performed three types of exoskeleton simulations. First, we simulated walking with time-periodic torques<sup>21,22</sup>, which simply used the equation 1 with the relevant torques; the torques used were zero everywhere, except for brief periods when the torque rose and fell linearly, resulting in a torque impulse (Figure 2D in the main manuscript). In this case, it is useful to the learner to include the relative perturbation timing from the exoskeleton as a sensed input state in addition to the biped state.

Second, we simulated walking with the torque impulse applied at specific leg angles, thereby making the exoskeleton assistance phase-periodic (Supplementary Fig. 4). This was achieved by starting the torque impulse at the desired leg angle via event detection in MATLAB.

Finally, we simulated the exoskeleton with assistance depending on step frequency<sup>23–25</sup>. In this case, the exoskeleton torque was constant over a step, and this constant was a function of the step frequency over the previous two steps. This simulation also involved a period where the walker's step frequency is constrained by a metronome, with the prescribed frequency changing providing the walker broad experience on the energy landscape. We simulated this metronome-constrained walking by pre-computing the walking gait at different frequencies and interpolating between them when a particular metronome frequency is commanded; see figure 4 of the main manuscript to see that this approach was satisfactory.

**Parameters.** The physical and metabolic parameters of the biped, as well as the parameters of the feedback controller were chosen independently of the adaptation experiments. Instead, they were fixed by using calculations from prior studies on the human walking steady state (Supplementary Figure 2)<sup>3–5,18</sup>. Aside from these parameters, the reinforcement learner has two parameters, the gradient descent learning rate  $\alpha_g$  and the finite memory size  $N_g$  used by the gradient estimator. The memory mechanism has two parameters: a learning rate for moving toward the memory  $\alpha_m$  and a learning rate for updating the memory  $\alpha_{\rm mf}$  toward the current controller. Unless otherwise stated, we usually used the following values for these parameters:  $\alpha_g = 1.2 \times 10^{-4}$ ,  $N_g = 30$ ,  $\alpha_m = 0.01$ , and  $\alpha_{\rm mf} = 0.03$ , all in non-dimensional terms. These values were not tuned based on

adaptation data, but instead were selected to simply demonstrate that the model predicts the many qualitative phenomena illustrated in the main manuscript figures 2, 4, 5, 6, and 7and Supplementary Figure 9). We confirmed that each of these parameters can generally be changed by at least 20% in each direction (and in many situations by a bigger factor) while retaining the general qualitative features of the predictions. The exploratory noise, in the absence of sensory noise was chosen to be  $2 \times 10^{-3}$  in the non-dimensional variables; the results are completely insensitive to this size in the linear regime of the dynamics, and the size primarily matters in comparison to the sensory noise (see Figure 4d in the main manuscript). The baseline sensory noise was multiplicative and only in the energy measurement: this baseline error standard deviation was  $10^{-4}$  (or 0.01%) times mean energy). In Figure 4d of the main manuscript, except for this baseline case, the other noise condition cases had both multiplicative noise scaling paramater. The noise range for was chosen to demonstrate how too much sensory noise may overwhelm the exploratory variability. For Figure 3of the main manuscript, we used additional sensory noise on the forward velocity, which is used by the feedback controller being tuned. Overall, because the experimental protocols differ widely even with a single paradigm such as split-belt walking and not all experimental details are typically published (e.g., accelerations when treadmill speeds are changed), we focus on predicting the qualitative features of the results rather than pursue a quantitative fit of the model to data or capturing the quantitative details of experimental protocols.

**Computational infrastructure.** The analysis was implemented in the widely-used scientific language MATLAB (version 2022a). Differential equations were simulated using ode45, with the event detection option to detect heel-strike and switch to the next step. For performing optimization calculations for fitting to data (not for simulating the 'learning'), we used fmincon in MATLAB. Simulation of learning is implemented as a stride-by-stride for-loop, in which the current control parameters are used to simulate one stride (two steps) and then the control parameters and the memory are changed according to the learning model outlined herein. Please code associated with this manuscript, LocAd<sup>26</sup>, available without restrictions in a public repository.

#### Further experimental and data details

For experimental work, we used the Vicon motion capture system with Vicon Nexus 1.x, Bertec instrumented split-belt treadmill, controlled from a MATLAB interface to automatically change speeds. As part of this study, we performed two split-belt walking experiments, involving a total of three conditions, with a total of 25 participants. The two experiments had 16 and 9 participants, and our participant number per condition was shown to be sufficient in prior split-belt studies for null hypothesis testing of difference in means (Torres-Oviedo and Bastian 2012, Malone Vasudevan and Bastian 2011). The resulting p-values were either less than 0.02 when 'significant' with a threshold of 0.05, or were greater than 0.3, so clearly insignificant. There were no marginal cases. No data were excluded from the analyses.

Statistical comparisons were performed for results in Figures 5, 6, 7 of the main manuscript. Normality of samples were tested using the Kolmogorov-Smirnov test, with a null hypothesis of normality and significance threshold for rejecting normality at the 0.05 level. The default statistical tests are *t*-tests, paired or unpaired as indicated when results are reported, allowing for unequal variances. Non-parametric tests were performed to augment the parametric t-tests: for such non-parametric tests, when the test is paired, we use a Wilcoxon signrank test and when the test is unpaired, we use a Wilcoxon ranksum test, also termed the Mann-Whitney U test. The non-parametric test always agreed with the parametric tests at the 0.05 threshold of significance. Model-based qualitative results reported in other figures are essentially deterministic and no statistical tests are necessary for these. The data were anonymized before analysis and the investigators were thus effectively blinded to group allocation (which was random). Because of the objective nature of the analyses, such blinding is not relevant to the interpretation of the results.

To illustrate whether model-based predictions agree qualitatively with experimental results in prior studies, data from prior manuscripts<sup>6,7,9,22,24,27–32</sup> were obtained by manual digitization and were plotted in Figures 2 and 7b and Supplementary Figures 2, 5, 6. This digitization is approximate and serves the purposes of qualitative comparisons.

#### Modulating memory use to not degrade via gradient descent

Consider the performance metric or objective function J(p) to be minimized and the following learning rule that combines gradient descent and progress toward memory:

$$p_{i+1} = p_i - \alpha_g \nabla_p J + \alpha_m (p_{\text{memory}} - p_i). \tag{7}$$

Here,  $\nabla_p J$  is the gradient of the objective *J* with respect to the variable *p*, when  $p = p_i$ . The stored motor memory  $p_{\text{memory}}$  need not necessarily be the correct minimum of the performance metric. Here, we first show why  $\alpha_m$  not being a constant is necessary, if this procedure must converge to an extremum of the objective. Next, we show that modulating  $\alpha_m$  via a truncated cosine tuning is sufficient to allow convergence to an extremum of the objective.

Feedback gain parameter $K_{ij}$	Value	Feedback gain parameter $K_{ij}$	Value
K <sub>11</sub>	-0.5211	K <sub>21</sub>	0.2793
K <sub>12</sub>	-0.0859	K <sub>22</sub>	-0.0290
K <sub>13</sub>	-0.0073	K <sub>23</sub>	0.0020
K <sub>14</sub>	-1.0559	K <sub>24</sub>	-0.0750

**Supplementary Table 2.** Parameters of the default feedback controller. Here,  $K_{jk}$  is defined as  $\Delta u_j/\Delta s_k$ , where *u* is the control and *s* is the state. For the control variable,  $u_1$  is the push-off and  $u_2$  is the swing leg angle at touch down. For the state variable  $s_1 = \dot{y}_{body/belt}$ ,  $s_2 = y_{body/ground}$ ,  $s_3 = \sum y_{body/ground}$ ,  $s_4 = \dot{y}_{body/ground} - \dot{y}_{body/belt}$ . All numbers are non-dimensional.

**Necessary condition.** Assume  $\alpha_m$  is constant. Fixed points  $p^*$  of equation 7 are given by when  $p_{i+1} = p_i = p^*$ . So, fixed points  $p^*$  satisfy:  $p^* = p^* - \alpha_g \nabla_p J(p^*) + \alpha_m (p_{\text{memory}} - p^*)$ , or

$$\alpha_g \nabla_p J(p^*) = \alpha_m (p_{\text{memory}} - p^*). \tag{8}$$

Thus, the only situation this procedure converges to an extremum of the objective at which the gradient equals zero  $(\nabla_p J(p^*) = 0)$  is in the special case where  $p_{\text{memory}}$  equals the optimum. For generic  $p_{\text{memory}}$  not equal to the optimum, the system will converge to a  $p^*$  such that the step along the negative gradient exactly cancels the step toward the memory, as in equation 8. Thus,  $\alpha_m$  cannot be constant and its modulation in *some* manner is necessary. This necessary modulation is not unique, and in the following paragraph, we prove the sufficiency of one such modulation.

**Sufficient condition.** Assume that  $\alpha_m = \alpha_0 h(\theta_{gm})$ , where  $\alpha_0$  is a constant and  $\theta_{gm}$  is the angle between the negative gradient  $-\nabla_p J$  and the current direction toward memory:  $p_{\text{memory}} - p$ . Say, the function  $h(\theta_{gm}) = 0$  when  $|\theta_{gm}| > 90$  degrees and  $h(\theta_{gm}) \neq 0$  when  $|\theta_{gm}| < 90$  degrees. One example of such a function *h* is a truncated cosine tuning, with  $h(\theta_{gm}) = 0$  when  $|\theta_{gm}| > 90$  degrees.

First, given the assumptions on  $h(\theta_{gm})$ , the iterations always proceeds along a descent direction, that is one that reduces the objective. This is true because:

- 1. when  $|\theta_{gm}| \ge 90$ , we have  $\alpha_m = 0$ , so the algorithm (equation 7) reduces to gradient descent and thus always steps along a descent direction;
- 2. when  $|\theta_{gm}| < 90$ , the step toward memory  $(p_{\text{memory}} p^*)$  has a positive component along the negative gradient by assumption of  $\theta_{gm}$ . Thus,  $(p_{\text{memory}} p^*)$  is a descent direction, and so the combined gradient descent step and the step toward memory in equation 7 is always a descent direction.

Second, given the assumptions on  $h(\theta_{gm})$ , we now show that  $p_{opt}$  with  $\nabla J = 0$  is a fixed point of the algorithm. Say there exists an optimal point  $p_{opt}$  where  $\nabla J = 0$  and  $p_{opt} \neq p_{memory}$ . Then, there exists an  $\varepsilon$  neighborhood S around  $p_{opt}$ , not containing  $p_{memory}$  which can be divided into two disjoint sets  $S_1$  and  $S_2$ , with  $p_{opt}$  being at the boundary separating  $S_1$  and  $S_2a$ with the two sets defined as follows. The set  $S_1$  is defined so that any point  $p \in S_1$  satisfies  $|\theta_{gm}| \ge 90$  degrees, so that when the current iterate falls in this region, the learning algorithm defaults to regular gradient descent because  $\alpha_m = 0$ . Thus, when the iterates  $p_i$  remain in  $S_1$ ,  $p^* = p_{opt}$  is an accumulation point of the iteration. The complementary set  $S_2$  is defined such that any point  $p \in S_2$  satisfies  $|\theta_{gm}| < 90$  degrees, but this set cannot contain any fixed points because  $|\theta_{gm}| < 90$  is incompatible with the fixed point equation  $-\alpha_g \nabla_p J(p) + \alpha_m (p_{memory} - p_i) = 0$ . This can be seen by taking the dot product of this fixed point equation with  $-\nabla_p J(p)$  and noting that the resulting scalar left hand side is non-negative and the right hand side is negative by definition. Thus, the only fixed point of the algorithm in the neighborhood of  $p_{opt}$  is  $p^* = p_{opt}$ , in the set  $S_1$ .

Thus, modulating the  $\alpha_m$  using a truncated cosine tuning is sufficient to ensure that (1) the algorithm always reduces the objective and (2) a fixed point of the descent algorithm is the optimal point  $p_{opt}$ . Of course, what we have shown does not guarantee convergence to a local minimum, which we leave for an examination in a future study.

#### Numerical experiments to show that delayed device response can degrade or stop optimization

In a number of exoskeleton adaptation experiments<sup>23,24,33,34</sup>, the assistance or resistance provided by the exoskeleton on one step depends on what the human did on the previous step (e.g., the previous step period or step width). Some treadmill adaptation studies also had a similar protocol<sup>35</sup>, the treadmill speed is based on previous step periods. At least in some of these studies<sup>23,24,33,34</sup>, many subjects did not initiate adaptation despite the obvious energetic advantage to such adaptation. Here, we argue that this non-adaptation could be due to the temporal delay between human action and the energetic reward or punishment. If the human nervous system is performing energy optimization based on correlating motor actions on a particular

step and their energetic consequences, we may expect such an energy optimization to fail when action and reward are separated. Indeed, there is some precedent for delay affecting motor control. However, the story is a bit more subtle and whether or not adaptation happens depends on the exploratory optimization algorithm and the exploration. Let us consider two example algorithms, including the algorithm we used. Say the goal is to find x to minimize the function f(x) and with  $x_0$  being the initial guess for the optimum. For simplicity, let us assume that the system has no additional dynamics.

Algorithm 1. Simplest hill climbing. While the term 'hill climbing' has sometimes been associated with gradient descent (more precisely, gradient ascent), here we refer to an even simpler local search algorithm<sup>23</sup>. Say the best guess for the optimum at step *i* is  $x_i$  with function value  $f(x_i)$ . The optimizer then evaluates the function at  $\hat{x}_{i+1} = x_i + \mu_i$ , that is, evaluates  $f(x_i + \mu_i)$ , where  $\mu_i$  is exploratory noise having Gaussian distribution and with the usual assumptions of Gaussian and independent from the previous  $\mu$ 's. The next best guess  $x_{i+1}$  of the optimum is decided by the following rule:

$$x_{i+1} = x_i + \mu_i \text{ if } f(x_i + \mu_i) < f(x_i)$$
(9)

$$x_{i+1} = x_i \text{ if } f(x_i + \mu_i) \ge f(x_i).$$
 (10)

That is, make a new guess; if the new guess improves the objective, go there; if not, stay where you are. It is well known that this algorithm goes toward local minima under normal circumstances. But if there is a 'delay' unbeknownst to the algorithm, for instance, wherein  $f(\hat{x}_{i+1})$  is actually  $f(\hat{x}_i)$ , then decisions to accept will be based on incorrect function values and it is clear that this algorithm will not be optimizing.

Algorithm 2. Gradient descent with isotropic exploration This is the gradient descent that we have used in this study, in which the gradient is estimated via linear regression between input and output over the past  $N_{\text{gradient}}$  steps. Here, the exploratory noise is isotropic, so all directions are equally likely. Without any delay between action x and function evaluation f, the algorithm reliably goes toward a local minimum. When there is a delay, the algorithm may sometimes go toward the optimum, thus 'adapting' and sometimes not make any progress, thus 'not adapting', even for the exact same values of all parameters, as shown in Fig. 10of the main manuscript. The reason the algorithm can sometimes go toward the optimum despite a delay is because the gradients on successive steps are correlated or persistent. Because successive steps are correlated, despite the function value mismatch, the algorithm can infer a reasonable descent direction as the gradient estimate, even if the gradient estimate may itself be biased.

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